

STRUCTURAL SEISMIC EVALUATION REPORT FOR:

WESTMORELAND ELEMENTARY SCHOOL PHASE 1

1717 City View St. Eugene, OR 97402 Lane Education Service District

PREPARED BY ZCS ENGINEERING & ARCHITECTURE

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Project Summary Information						
Building Part	Building Part Name	Included in Retrofit	Year Built	Building Type***	Nonstructural Retrofits Included in Scope Y/N***	Previous Seismic Retrofit Y/N*** (Year if Yes)
А	Classrooms	No	1950			
В	Gymnasium	No	1950			
С	Classrooms	Yes	1950	W2	Y	N
D	Classrooms	Yes	1950	W2	Y	N
E	Cafeteria	Yes	1950			
F	Classrooms	Yes	1950			
G	Boiler Room	Yes	1950			
	tural deficienci		• •		d in proposed s I ST be included	eismic retrofit in the scope of work
	••••	•		•••		retrofits MUST be ra building part.
Total Ret	trofit Cost	\$2,378,36	65			
Retrofit S	Square Feet	17,550				
Retrofit Cost perSquare Foot\$135.52						
Is the car instability		otential or			andslide/slope d area? If so,	Yes, see Appendix B

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1.0 Executive Summary

The Lane Education Service District is located in Eugene, Oregon in Lane County. The District operates 1 school located within the community including the property of interest, Westmoreland Elementary School located in the city of Eugene, Oregon. The District has retained ZCS Engineering and Architecture (ZCS) to perform a seismic evaluation of Westmoreland Elementary School that provides the District with an objective, comprehensive analysis of the condition of the building's seismic resisting systems. The purpose of the evaluation is to determine the seismic lateral resisting system deficiencies when compared to buildings designed using modern building codes. This evaluation was performed in accordance with the American Society of Civil Engineers "Seismic Rehabilitation of Existing Buildings ASCE/SEI 41-17".

Westmoreland Elementary School is located at 1717 City View Street in Eugene, Oregon (See Sheet G0.0 – Vicinity Map). ZCS was tasked with evaluating the lateral force resisting systems of the structures located on the site. The structures evaluated as part of this report include several classroom buildings. All the structures included in the scope of this seismic evaluation report are constructed of straight sheathed shear walls supporting straight sheathed diaphragms. Additionally, the buildings included in the scope of this evaluation have masonry veneers around the exterior walls. The total building area included in this evaluation is approximately 18,250 square feet.

The evaluation of the facility indicates, rehabilitation of existing lateral system components is necessary to meet the following requirements as outlined in ASCE 41-17:

- School buildings, other than areas which may be used as emergency shelters, shall be categorized as Risk Category III and evaluated to meet the Limited Safety structural performance and Hazards Reduced nonstructural performance level for BSE-2E loading.
- School areas that may be used as emergency shelters shall be categorized as Risk Category IV and evaluated to meet:
 - The Life Safety structural performance and Hazards Reduced nonstructural performance level for BSE-2E level, AND
 - The Immediate Occupancy structural performance and Position Retention nonstructural performance level for BSE-1E level.

See section 3.2 for performance level definitions.

The following is a brief list of structural deficiencies encountered:

- No continuous load path exists between roof diaphragm and foundation elements
- Straight sheathed shear walls are not adequate to resist in-plane forces
- Sill plates are not adequately anchored to foundation elements
- Straight sheathed diaphragms exceed maximum allowable spans
- Shear walls do not meet the required aspect ratios

Recommendations mitigating the known deficiencies determined by our analysis are outlined in section 4.0 of this report. In addition to the rehabilitation recommendations, we prepared schematic seismic retrofit drawings to convey the intent of the rehabilitation effort. These drawings are included in Appendix E.

To help the District understand the magnitude of the rehabilitation effort and secure funding sources for the seismic system rehabilitation of the building, a preliminary construction cost estimate was developed. With the assistance of a seismic retrofit contractor a total construction cost of **\$2,378,365** including all soft costs associated with architecture/engineering, permitting, and District Project Management was developed. Refer to section 5.0 of the report body.

In addition to the construction cost estimation efforts we performed a "Benefit Cost Analysis" using the tool provided by the State of Oregon Infrastructure Finance Authority. The building has a benefit cost score of **0.301**. Refer to Appendix D for BCA worksheets.

The cafeteria and school buildings are of significant importance to the community, as well as neighboring communities in Lane County. During a seismic event, the cafeteria is large enough to serve as an emergency shelter for both the school and the surrounding neighborhood. The current lateral force resisting system does not meet the current prescribed seismic requirements and may not be suitable for use as a shelter after a seismic event. In addition to the emergency shelter, Lane School educates disadvantaged students from around Lane County that are require additional social, emotional, and/or behavioral support. Because of the wide area of service, many different communities in Lane County will benefit from seismic upgrades to this site. The structural and nonstructural deficiencies present in the buildings would likely be the cause of significant damage to the structure but would be rectified with the assistance of this grant, allowing the buildings to perform well in a seismic event.

It is our final recommendation that given the BCA score and the general condition of the seismic resisting systems, this building is an excellent candidate to be rehabilitated to meet the currently prescribed seismic demands for Limited Safety (BSE-2E), Damage Control (BSE-1E), Life Safety (BSE-2E), and Immediate Occupancy (BSE-1E) per ASCE 41-17, as applicable. Once rehabilitated, this building will meet the needs of the District and community for future generations.

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2.0 Project Introduction

Lane Education Service District is centrally located in Eugene, Oregon in Lane County. Westmoreland Elementary School is located at 1717 City View Street in Eugene, Oregon (See Sheet G0.0 – Vicinity Map).

The District has retained ZCS Engineering and Architecture (ZCS) to perform a seismic evaluation of Westmoreland Elementary School. The purpose of the evaluation is to provide the District with an objective, comprehensive analysis of the condition of the existing seismic force resisting systems of the facility when compared to a building constructed using modern building codes. In addition to evaluating the building's seismic performance, schematic seismic retrofit plans have been developed. The rehabilitation plans have been developed using our extensive knowledge of seismic rehabilitation and are intended to meet the objectives and the level of performance of Limited Safety (BSE-2E), Damage Control (BSE-1E), Life Safety (BSE-2E), and Immediate Occupancy (BSE-1E) based on the ASCE 41-17 requirements, as applicable. Based on the seismic evaluation and schematic rehabilitation design drawings, a preliminary construction cost estimate was developed. Based on the preliminary construction cost estimate was prepared to help the District determine whether or not the rehabilitation efforts outlined in this report are financially responsible.

This work was conducted at the request of Brad Johnston, Facilities Manager, under an engineering services contract between the District and ZCS.

2.1 Scope of Work

The following scope of work was developed to meet the objectives outlined above.

Seismic Evaluation & Preliminary Rehabilitation Services:

- Review original building construction drawings to determine existing structural systems and areas of concern.
- Perform site visits of the structure to observe structural systems and visually review structural condition and deficiencies.
- Observe lateral system (seismic) components and load path.
- Observe gravity system components and load path.
- Observe for damage and failing elements.
- Develop schematic level as-builts based on site measurements.
- Evaluate existing construction based on visual observations and available asconstructed documentation against ASCE 41-17 Tier 1 requirements.
- Collate findings and perform preliminary calculations to assist in the determination of each building's seismic deficiencies.

• Prepare an evaluation report for the facility identifying the structural integrity and seismic deficiencies stamped by a registered Structural Engineer licensed in the State of Oregon.

Preliminary Construction Cost Consulting Services:

- Develop project base sheets based on the District provided original drawings and ZCS developed as-builts.
- Prepare conceptual rehabilitation drawings based on ASCE 41 guidelines to convey the intent of rehabilitation recommendations.
- Prepare a project cost estimate based on historic projects of similar scope and magnitude.
- Review constructability and cost estimate with a licensed contractor.
- Revise plans based on contractor input as required to optimize the efficiency of the rehabilitation plan and develop final construction cost recommendations.
- Prepare cost benefit analysis based on SRGP methodologies
 *Financial and enrollment information has been provided by the District
- Summarize findings in final report package stamped by a registered Structural Engineer licensed in the State of Oregon.

3.0 Structural Evaluation

3.1 Introduction

ZCS was tasked with evaluating the lateral force resisting systems of the structures located on the site. The structures evaluated as part of this report include several classroom buildings. All the structures included in the scope of this seismic evaluation report are constructed of straight sheathed shear walls supporting straight sheathed diaphragms. Additionally, the buildings included in the scope of this evaluation have masonry veneers around the exterior walls. The total building area included in this evaluation is approximately 18,250 square feet.

3.2 Structural Evaluation

The following outlines the evaluation of the existing structural components of the building. The evaluation includes site observations of the existing structural elements and follows the guidelines outlined in the American Society of Civil Engineer's "Seismic Evaluation of Existing Buildings – ASCE 41-17". This manual is the required evaluation tool per the Seismic Rehabilitation Grant Program through Business Oregon Infrastructure Finance Authority. Per ASCE 41-17 a Tier 1 evaluation has been performed. The purpose of a Tier 1 evaluation is to provide "Quick Checks" to properly evaluate a building and determine deficiencies related to the lateral resisting elements.

It is the intent of the District, as part of this study, to determine the structural deficiencies of the building as compared to current prescribed loading and detailing requirements for lateral (wind/seismic) loading to a performance level of "Limited Safety (BSE-2E)" per ASCE 41-17. The level of performance is defined per ASCE 41-17 as:

"The Limited Safety Structural Performance Level is set forth as a midway point between Life Safety and Collapse Prevention. It is intended to provide a structure with a greater reliability of resisting collapse than a structure that only meets the Collapse Prevention Performance Level, but not to the full level of safety that the Life Safety Performance Level would imply."

"Structural Performance Level S-3, Life Safety, means the post-earthquake damage state in which significant damage to the structure has occurred but some margin against either partial or total structural collapse remains. Some structural elements and components are severely damaged, but this damage has not resulted in large falling debris hazards, either inside or outside the building. Injuries might occur during the earthquake; however, the overall risk of life-threatening injury as a result of structural damage is expected to be low. It should be possible to repair the structure; however, for economic reasons, this repair might not be practical. Although the damaged structure is not an imminent collapse risk, it would be prudent to implement structural repairs or install temporary bracing before reoccupancy."

"Structural Performance Level, Collapse Prevention, means the post-earthquake damage state in which the building is on the verge of partial or total collapse. Substantial damage to the structure has occurred, potentially including significant degradation in the stiffness and strength of the lateral-force-resisting system, large permanent lateral deformation of the structure, and to a more limited extent - degradation in vertical-load-carrying capacity. However, all significant components of the gravity-load-resisting system must continue to carry their gravity loads. Significant risk of injury caused by falling hazards from structural debris might exist. The structure might not be technically practical to repair and is not safe for reoccupancy because after shock activity could induce collapse."

Per ASCE 41-17 a seismic hazard level is required. In order to obtain a performance level of "Limited Safety" the seismic hazard shall be BSE-2E as defined in section 2.4.1.3 and C2.4.1.3. The BSE-2E hazard level earthquake has a probability of occurring once in every 975 years, or 5% chance in 50 years. This design level earthquake represents ground motions approximately 75% as large as those prescribed for new buildings. We feel this provides an appropriate level of performance for this facility.

Lateral resisting systems work in conjunction with gravity framing systems. As such, the existing gravity framing system was also reviewed for structural deficiencies during our site observations. Section 3.2.3 outlines the existing gravity system and its structural deficiencies found during the evaluation.

Geologic hazards were assessed as part of our engineering evaluation. The main hazards evaluated in our analysis included liquefaction, slope failure, and surface fault rupture potential. These potential hazards were evaluated using ASCE 41-17 guidelines, as well as information provided by the online Oregon HazVu: Statewide Geohazards Viewer, maintained by DOGAMI. Results from the HazVu analysis are included in Appendix B.

3.2.1 Lateral Resisting Systems

After reviewing the facility and the existing drawings we have determined the lateral system is defined as a commercial/industrial wood framed construction for the classroom buildings and as unreinforced masonry for the boiler room. Per ASCE 41, commercial/industrial wood framed and unreinforced masonry bearing wall lateral systems are defined as:

Wood Frames, Commercial and Industrial W2 – These buildings are commercial or industrial buildings with a floor area of 5,000 ft² or more. There are few, if any, interior walls. The floor and roof framing consist of wood or steel trusses, glulam or steel beams, and wood posts or steel columns. The foundation system may consist of a variety of elements. Seismic forces are resisted by wood diaphragms and exterior stud walls sheathed with plywood, oriented strand board, stucco, plaster, or straight or diagonal wood sheathing, or they may be braced with rod bracing. Wall openings for storefronts and garages, where present, are framed by a post-and-beam framing.

3.2.2 Lateral Resisting System Deficiencies

The following lateral resisting element deficiencies are based on visual observations of the existing structural elements and the structural analysis performed during the Tier 1 "Quick Checks" of the ASCE 41-17. The Tier 1 checklists are attached in Appendix B. The following outlines the deficiencies for each portion of the facility.

- S1. Roof diaphragm is not properly attached to foundation elements to transfer out-ofplane loads.
- S2. Adjacent buildings are not restrained to limit pounding effects.
- S3. Seismic force resisting elements are not continuous to foundation at window openings.
- S4. Plan irregularities create torsional effects under seismic loading.
- S5. DOGMAI HazVu maps indicate the potential of liquefaction hazards.
- S6. Straight sheathed shear walls are not adequate to resist in-plane forces.
- S7. Straight sheathed shear walls do not meet required aspect ratios.
- S8. No wood structural panel shear walls or alternative construction to transfer forces across openings.
- S9. No positive connections provided at posts to foundation elements.
- S10. Sill plates are not adequately anchored to foundation elements.
- S11. No positive connections provided at girder to columns.
- S12. Straight sheathed diaphragms exceed maximum allowable span limits.
- S13. Diaphragms exceed maximum allowable spans.

3.2.3 Gravity Resisting Systems and General Observations

The following gravity resisting deficiencies are based on visual observations of the existing structural elements. No formal structural analysis was performed during this evaluation of the gravity resisting elements.

- No known gravity deficiencies were observed.
- The gravity resisting system was found to be in good general condition based on the visual observations performed.

3.2.4 Evaluation of Incidental Items

Incidental, non-structural, items can play a major role in the overall expense of rehabilitating an existing building. These costs can be significant and can be very difficult to estimate prior to construction. The following is a list of the specific deficiencies noted during an on-site visit.

- N1. Pipes conveying natural gas are not adequately restrained.
- N2. Verification is needed to determine if shutoff valves are present.
- N3. Flexible couplings are not provided on natural gas piping.
- N4. Tops of interior partition walls are not adequately attached to the diaphragms.
- N5. Supports for large piping are not restrained to prevent failure.
- N6. Masonry veneer adjacent to egress paths is not adequately tied to structure.
- N7. Masonry veneer is not anchored to the backup adjacent to weakened planes.
- N8. Weep holes are not present in some of the masonry veneer.
- N9. Covered walkway canopies are not adequately braced to structure.
- N10. Shelving units are not restrained to resist overturning forces.
- N11. Items and mechanical units more than 4ft above floor level are not adequately restrained.
- N12. Large equipment is not anchored to structure to prevent overturning.

Based upon ZCS's previous experience the buildings contain some form of hazardous material. These materials will need to be dealt with on a case-by-case basis as they are encountered during the project.

4.0 Seismic Rehabilitation Recommendations

The following structural improvements are required to resolve the lateral force resisting system deficiencies noted in section 3.2.2. These improvements are detailed below and in the attached schematic seismic rehabilitation drawings found in Appendix E. The attached drawings were prepared to assist in defining the rehabilitation scope of work.

4.0.1 Rehabilitation Recommendations for Lateral Resisting Elements (See Section 3.2.2)

- S1. Provide new blocking, clipping, and nailing to establish adequate connection of the roof diaphragm to foundation elements.
- S2. Restrain adjacent buildings using blocking and strapping, as required, to prevent pounding.
- S3. Ensure seismic force resisting elements provide a positive connection between roof diaphragm and foundation levels.
- S4. Provide blocking and strapping at reentrant corners of diaphragm to strengthen framing around torsional irregularities.
- S5. Underpin existing foundation elements with micropile where liquefaction hazards exist.
- S6. Provide new plywood sheathing over existing straight sheathed walls to increase in-plane shear capacity.
- S7. Infill existing wall penetrations to bring shear wall aspect ratios to within the allowable limits.
- S8. Provide new plywood sheathing or alternative construction methods to infill existing windows and allow for the transfer of shear forces across window openings.
- S9. Provide new hardware to positively attach wood posts to foundation elements and allow for the transfer of shear forces.
- S10. Provide new sill plate anchor bolts to positively attach structure to foundation elements and allow for transfer of shear forces.
- S11. Provide new connection hardware at girder to column connections that are adequate for transfer of shear forces.
- S12. Provide new plywood sheathing over existing straight sheathed diaphragms to increase maximum allowable spans.
- S13. Provide additional diaphragm attachments and/or block panel edges to reduce span lengths to allowable limits.

4.0.2 Rehabilitation Recommendations for Gravity Resisting Systems and General Observations (See Section 3.2.3)

• Rehabilitation of the gravity resisting system is not required at this time.

4.0.3 Rehabilitation Recommendations for Incidental Items (See Section 3.2.4)

- N1. Properly brace all existing fluid piping, ducting, and any gas piping as required.
- N2. Verify installation of emergency shut off valves for gas utilities.
- N3. Provide flexible couplings on natural gas and fluid piping to allow for deflection in seismic events.
- N4. Provide proper attachment and bracing for all non-structural walls and partitions.
- N5. Properly brace all existing fluid piping, ducting, and any gas supports as required.
- N6. The brick veneer over the exit doors and egress paths will be anchored to the wood walls to minimize the falling hazard.
- N7. Anchor masonry veneer to backup adjacent to weakened planes.
- N8. Ensure weep holes in masonry veneer are present and clean of debris.
- N9. Properly attach covered walkway canopies to adjacent structures and the specified minimum spacing and provide new cantilever columns for in-plane forces
- N10. Properly brace tall-narrow shelving units and equipment to resist overturning forces
- N11. Any items (including mechanical units) weighing over 20 lbs. and above 4', and all equipment over 100 lbs. shall be attached and properly braced.
- N12. All equipment over 400 lbs. shall be anchored to structure.



5.0 Preliminary Construction Cost Estimate

The attached engineer's opinion of probable cost has been developed by ZCS for Westmoreland Elementary School. ZCS has a successful record of completing seismic rehabilitation projects within the State of Oregon. The prices provided in the attached cost estimate have been developed using the extensive list of past projects as a baseline for this project. These prices are based on Oregon BOLI wage rates. The cost estimate is broken down into multiple line items associated with each major task (general conditions, foundation, structural steel, MEP, etc) associated with the rehabilitation. Additional line items are included for design associated permit costs, and owner construction management.

The generation of the preliminary construction cost estimate line item costs were reviewed with a local construction company representative who has participated in similar construction projects. This representative is a highly qualified commercial contractor that has worked on multiple essential facilities and performed seismic retrofits to existing structures. They reviewed the values presented in the construction cost estimate and provided insight into current construction costs from a contractor's perspective. After final review the preliminary opinion of probable cost is **\$2,378,365**.

The engineer responsible for the evaluation of the building and design of the retrofit scheme has reviewed the cost estimate and deemed it to be valid and accurate. The cost estimate includes mitigation of all the seismic deficiencies in the retrofit scope of work through inclusion of scope of work elements identified in the report and plans. To the best of our knowledge, based on known and readily identifiable existing conditions, the cost estimate is all inclusive of items required to perform the retrofit and will result in a project that can be constructed within the proposed budget.

6.0 Benefit Cost Analysis

The provided benefit-cost analysis (BCA) included in Appendix D, has been prepared by ZCS using the BCA tool as provided by the State of Oregon Infrastructure Finance Authority. The costs associated with the building replacement value, contents replacement value, and occupancy values have been developed by District staff using recent data.

The Westmoreland Elementary School was surveyed during the statewide assessment of emergency buildings performed by Department of Geology, Mineral and Industries' (DOGAMI) Rapid Visual Screening (RVS) process in 2005 as part of senate bill 2. The occupancy and budget data provided by the District is for the entire school campus.

The BCA for this project is **0.301**. Given the BCA score of **0.301** is less than 1.0, we still recommend the proposed seismic retrofit and feel this building is a great candidate for the grant given its importance to the community it serves.

7.0 Conclusion and Recommendations

The findings described in this report have been limited to the lateral force-resisting structural system and general assessment of the gravity force-resisting elements. Based on our visual observations, we find the structure to be in good condition and generally safe for occupancy. No significant damage to the existing structural system was discovered.

Given the current condition of the structure, the current code section on existing buildings does not mandate that upgrades are required unless the building is scheduled for repairs, alterations, additions, or change in occupancy. However, it is our understanding the goal of the District is to continue utilizing the existing buildings as classrooms and cafeteria, and the District wants the seismic structural system to be compliant with the current code. To clarify, upgrades outlined in this report are strictly at the discretion of the District.

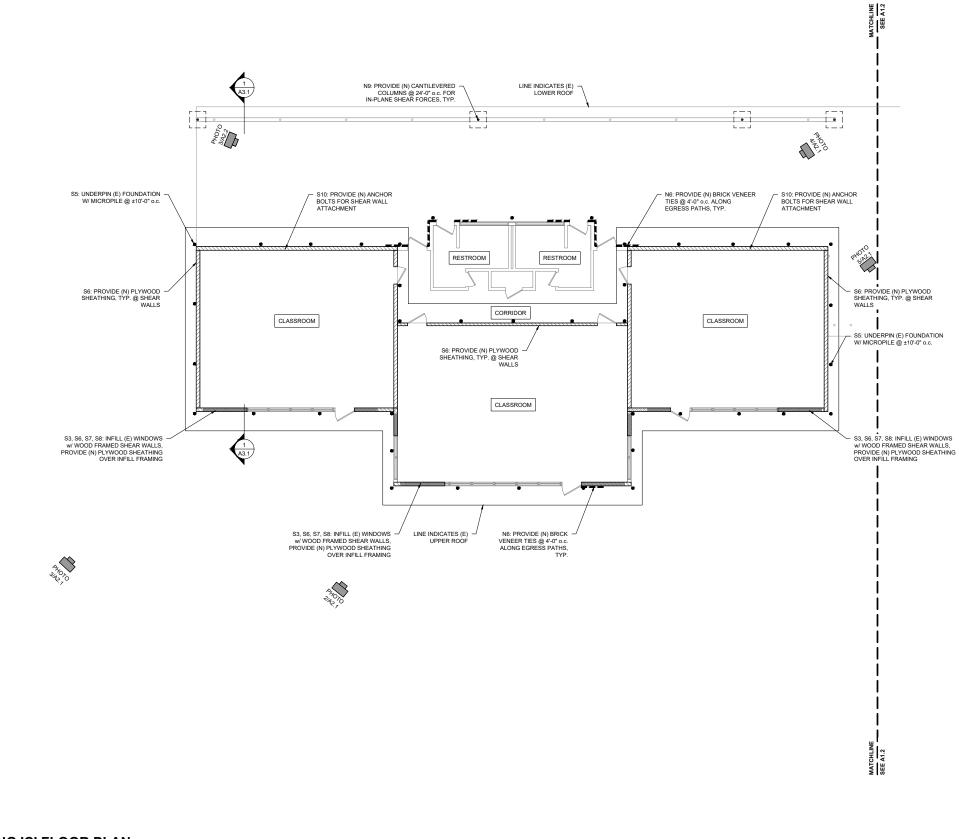
We have attempted to identify all areas requiring upgrades to achieve a scope of work for current code compliance, associated estimated costs and project schedule.

Please contact our office if you would like to discuss our findings. Please review the attached schematic drawings that can be used to refine a scope and budget.



Appendix A: Figures

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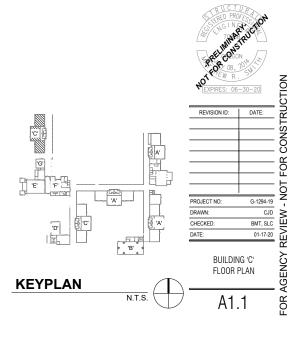
1 BUILDING 'C' FLOOR PLAN



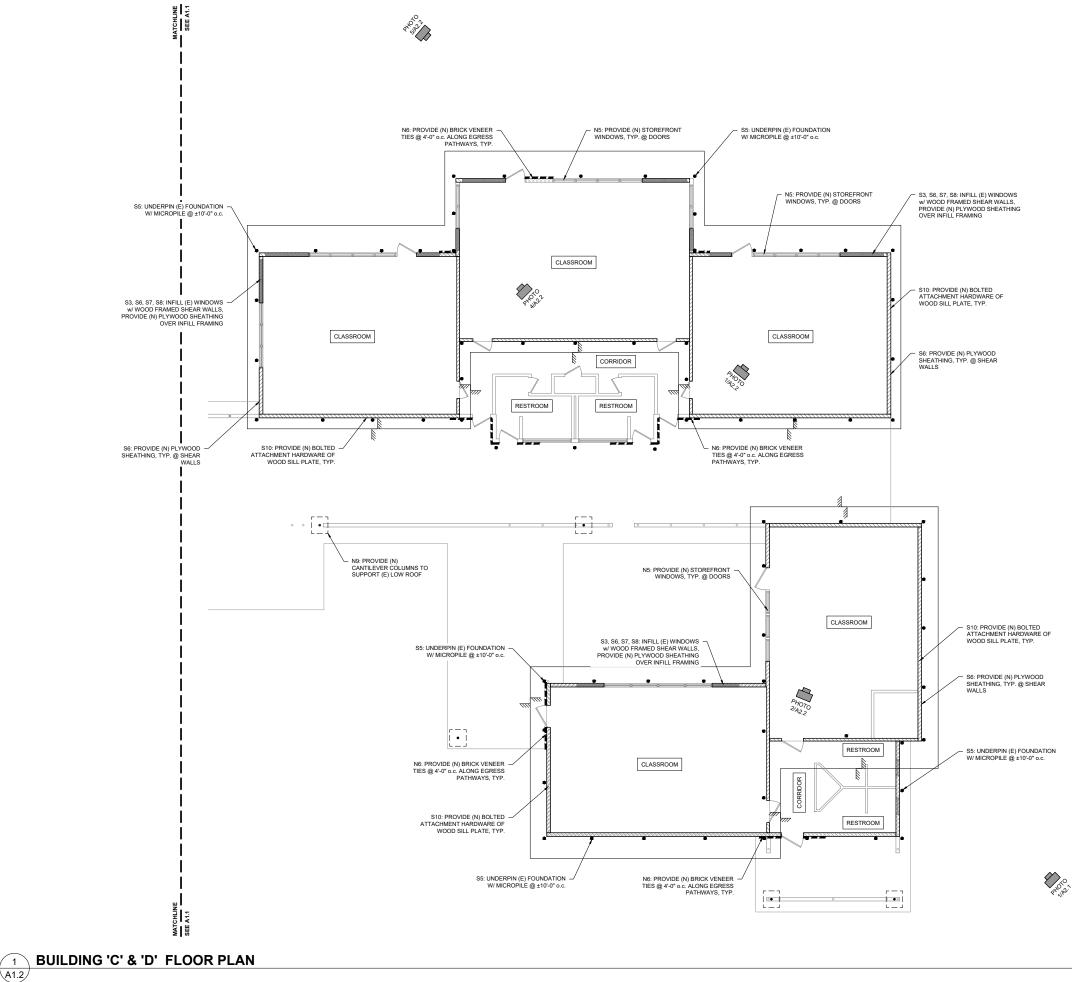
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LANE ESD 1200 HIGHWAY 99 NORTH EUGENE, OREGON 97402









A1.2

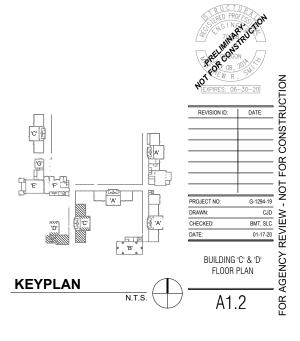
1/8" = 1'-0"



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LANE ESD 1200 HIGHWAY 99 NORTH EUGENE, OREGON 97402













3 PHOTO A2.1



PHOTO A2.1







N.T.S.



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LANE ESD 1200 HIGHWAY 99 NORTH EUGENE, OREGON 97402













3 PHOTO

N.T.S.



2 PHOTO A2.2







N.T.S.

N.T.S.



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Appendix B: Structural Tier 1 Check Sheets

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Tier 1 Deficiency Summary							
Deficiency Number(s)							
	Per Sections 3.2.2 - 3.2.4						
Noncompliant Item in Tier 1	& Retrofit Drawings	Comments					
	Buildings C and D						
Table 17-1. Very Low Seismicity C	<u>hecklist</u>						
Structural Components	Structural Components						
No continuous load path between roof							
LOAD PATH S1 diaphragm and foundation elements							

Table 17-2. Collapse Prevention Basic Configuration Checklist					
Low Seismicity					
Building System—General					
LOAD PATH	S1	No continuous load path between roof diaphragm and foundation elements			
ADJACENT BUILDINGS	S2	Adjacent buildings are not restrained to limit pounding effects			
Building System—Building Configura	tion				
VERTICAL IRREGULARITIES	S3	Seismic force resisting elements are not continuous to foundation			
Moderate Seismicity					
Geologic Site Hazards					
LIQUEFACTION	S5	DOGAMI HazVu maps indicate potential liquefaction hazards			

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Table 17-6. Collapse Prevention Structu	ural Checklist for B	Building Type W2
Low and Moderate Seismicity		
Seismic-Force-Resisting System		
		Straight sheathed shear walls are not
SHEAR STRESS CHECK	S6	adequate to resist in-plane forces
		Straight sheathed shear walls do not
NARROW WOOD SHEAR WALLS	S7	meet required aspect ratios
		No wood structural panel shear walls or
		alternative construction to transfer
OPENINGS	S8	forces across window openings
Connections		
		No positive connections provided at
WOOD POSTS	S9	columns to foundation elements
		Sill plates are not adequately anchored
WOOD SILLS	S10	to foundation elements
		No positive connections provided at
GIRDER-COLUMN CONNECTION	S11	girder to column connection
High Seismicity		
Connections		
		Sill plates are not adequately anchored
WOOD SILL BOLTS	S10	to foundation elements
Diaphragms		
		Straight sheathed diaphragms exceed
STRAIGHT SHEATHING	S12	maximum allowable span limits
		Diaphragms exceed maximum allowable
SPANS	S13	spans limits

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Table 17-38. Nonstructural Checklist		
Hazardous Materials		
HAZARDOUS MATERIAL		Pipes conveying natural gas are not
DISTRIBUTION	N1	adequately restrained
		Verification is needed to determine if
SHUTOFF VALVES	N2	shutoff valves are present
		Flexible couplings are not provided on
FLEXIBLE COUPLINGS	N3	natural gas piping
Partitions		
		Tops of interior partition walls are not
TOPS	N4	adequately attached to the diaphragms
Masonry Veneer		
		Masonry veneer adjacent to egress paths
TIES	N6	is not adequately tied to structure
		Masonry veneer is not anchored to the
WEAKENED PLANES	N7	backup adjacent to weakened planes
		Weep holes are not present in some of
WEEP HOLES	N8	the masonry veneer
Parapets, Cornices, Ornamentation,	and Appendages	
		Covered walkway canopies are not
CANOPIES	N9	adequately restrained
Contents and Furnishings		
		Shelving units are not restrained to resist
TALL NARROW CONTENTS	N10	overturning forces
		Items more than 4ft above floor level are
FALL-PRONE CONTENTS	N11	not adequately restrained
Mechanical and Electrical Equipmen	t	
		Mechanical units are not adequately
FALL-PRONE EQUIPMENT	N11	braced to structure
		Equipment is not braced to resist
TALL NARROW EQUIPMENT	N10	overturning forces
		Large equipment is not anchored to
HEAVY EQUIPMENT	N12	structure
Piping		
		Flexible couplings are not provided on
FLEXIBLE COUPLINGS	N3	natural gas or fluid piping
		Pipes conveying fluids and natural gas
FLUID AND GAS PIPING	N1	are not adequately restrained
		Supports for large piping are not
C-CLAMPS	N13	restrained

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Appendix C: Summary Data Sheet

BUILDING DATA Building Name: WESTMORELAND CAM				Date: 11/7/2019
Building Address: 1717 CITY VIEW ST				
Latitude: <u>44.041151</u>		gitude: -123.126688		By: BMT
Year Built: 1950s (EST.)	Year(s) Remo	deled:	Original Desigr	n Code:
Area (sf): ± 8,330 (4,165 EA		th (ft): ± 120		dth (ft): ± 38
No. of Stories: 1	Story H			Height: ± 10 FT
USE Industrial Office	Warehouse	Hospital 🔲 Reside	ential 🗹 Educational	□ Other:
CONSTRUCTION DATA				
Gravity Load Structural System:	WOOD FRAMED BEA	RING WALLS W/ FLEXI	BLE ROOF DIAPHRAGM ON	TIMBER TRUSS SYSTEM
Exterior Transverse Walls:	WOOD FRAMED BEA	RING WALLS	Opening	js? YES
Exterior Longitudinal Walls:	WOOD FRAMED BEA	RING WALLS	Opening	ys? YES
Roof Materials/Framing:	BUILT-UP (B) OR TPO	OVERLAY (E) ABOVE	2x TRUSS FRAMING W/ STR	RAIGHT SHEATHING
Intermediate Floors/Framing:	N/A			
Ground Floor:	SLAB ON GRADE			
Columns:	TIMBER		Foundati	on: CONT. CONCRETE
General Condition of Structure:	FAIR			
Levels Below Grade?	NONE			
Special Features and Comments:	MASONRY VENEER			
LATERAL-FORCE-RESIST				<u> </u>
		Longitudinal		Transverse
System:	WOOD FRAMED S	HEAR WALLS	WOOD FRAM	1ED SHEAR WALLS
Vertical Elements:	WOOD FRAMED B	EARING WALLS	WOOD FRAM	1ED BEARING WALLS
Diaphragms:	STRAIGHT SHEAT	HED	STRAIGHT S	HEATHED
Connections:	POSITIVE AND FR	ICTION	POSITIVE AN	ID FRICTION
EVALUATION DATA				
BSE-1N Spectral Res Acceler		_ 0.588	S _{D1} =	
	actors: Class	= D	F _a =	1.223 F _v =
BSE-2E Spectral Res Acceler		= 0.693	S _{X1} =	0.569
Level of Seis		HIGH	Performance Level:	LIMITED SAFETY (S-4)
Building	Period: 7	= 0.16		
Spectral Accele	eration: S _a	= 0.693		
Modification	Factor: $C_m C_1 C_2$	= 1.3 (TABLE 4-7)	Building Weight: W=	± 260.6 KIPS (EACH)
Pseudo Lateral	Force: $C_m C_1 C_2 S_a W$			
BUILDING CLASSIFICATIO	N: <u>W2</u>			
REQUIRED TIER 1 CHECK	LISTS	Yes	No	
Basic Configuration Checklist				
Building Type W2 Structural Ch	necklist			
Nonstructural Component Chec	klist	 ✓ 		
FURTHER EVALUATION R	EQUIREMENT: _			

Table 17-1. Very Low Seismicity Checklist

Status	Evaluation Statement	Tier 2 Reference	Commentary Reference
Structural Co	nponents		
CNCN/A U	LOAD PATH: The structure contains a complete, well-defined load path, including structural elements and connections, that serves to transfer the inertial forces associated with the mass of all elements of the building to the foundation.	5.4.1.1	A.2.1.1
C NC 🕪 U	WALL ANCHORAGE: Exterior concrete or masonry walls that are dependent on the diaphragm for lateral support are anchored for out-of-plane forces at each diaphragm level with steel anchors, reinforcing dowels, or straps that are developed into the diaphragm. Connections have adequate strength to resist the connection force calculated in the Quick Check procedure of Section 4.4.3.7.	5.7.1.1	A.5.1.1

Note: C = Compliant, NC = Noncompliant, N/A = Not Applicable, and U = Unknown.

Table 17-2. Collapse Prevention Basic Configuration Checklist

Status	Evaluation Statement	Tier 2 Reference	Commentary Reference
Low Seismici			
Building Syst			
C (NC) N/A U	LOAD PATH: The structure contains a complete, well-defined load path, including structural elements and connections, that serves to transfer the inertial forces associated with the mass of all elements of the building to the foundation.	5.4.1.1	A.2.1.1
CNCN/A U	ADJACENT BUILDINGS: The clear distance between the building being evaluated and any adjacent building is greater than 0.25% of the height of the shorter building in low seismicity, 0.5% in moderate seismicity, and 1.5% in high seismicity.	5.4.1.2	A.2.1.2
C NC <mark>N/A</mark> U	MEZZANINES: Interior mezzanine levels are braced independently from the main structure or are anchored to the seismic-force-resisting elements of the main structure.	5.4.1.3	A.2.1.3
	em—Building Configuration		
C NC (\/A) U	WEAK STORY: The sum of the shear strengths of the seismic-force-resisting system in any story in each direction is not less than 80% of the strength in the adjacent story above.	5.4.2.1	A.2.2.2
C NC 🗤 U	SOFT STORY: The stiffness of the seismic-force-resisting system in any story is not less than 70% of the seismic-force-resisting system stiffness in an adjacent story above or less than 80% of the average seismic-force-resisting system stiffness of the three stories above.	5.4.2.2	A.2.2.3
C NC N/A U	VERTICAL IRREGULARITIES: All vertical elements in the seismic-force- resisting system are continuous to the foundation.	5.4.2.3	A.2.2.4
	GEOMETRY: There are no changes in the net horizontal dimension of the seismic-force-resisting system of more than 30% in a story relative to adjacent stories, excluding one-story penthouses and mezzanines.	5.4.2.4	A.2.2.5
	MASS: There is no change in effective mass of more than 50% from one story to the next. Light roofs, penthouses, and mezzanines need not be considered.	5.4.2.5	A.2.2.6
C NC N/A U	TORSION: The estimated distance between the story center of mass and the story center of rigidity is less than 20% of the building width in either plan dimension.	5.4.2.6	A.2.2.7

Table 17-2 (Continued). Collapse Prevention Basic Configuration Checklist

Status	Evaluation Statement	Tier 2 Reference	Commentary Reference
	smicity (Complete the Following Items in Addition to the Items for Low Seism	nicity)	
Geologic Site	Hazards		
	LIQUEFACTION: Liquefaction-susceptible, saturated, loose granular soils that could jeopardize the building's seismic performance do not exist in the foundation soils at depths within 50 ft (15.2 m) under the building.	5.4.3.1	A.6.1.1
CNC N/A U	SLOPE FAILURE: The building site is located away from potential earthquake- induced slope failures or rockfalls so that it is unaffected by such failures or is capable of accommodating any predicted movements without failure.	5.4.3.1	A.6.1.2
CNC N/A U	SURFACE FAULT RUPTURE: Surface fault rupture and surface displacement at the building site are not anticipated.	5.4.3.1	A.6.1.3
High Seismici	ty (Complete the Following Items in Addition to the Items for Moderate Seisn	nicity)	
Foundation C			
CNC N/A U	OVERTURNING: The ratio of the least horizontal dimension of the seismic-force- resisting system at the foundation level to the building height (base/height) is greater than 0.6 <i>S</i> _a .	5.4.3.3	A.6.2.1
CNC N/A U	TIES BETWEEN FOUNDATION ELEMENTS: The foundation has ties adequate to resist seismic forces where footings, piles, and piers are not restrained by beams, slabs, or soils classified as Site Class A, B, or C.	5.4.3.4	A.6.2.2

Note: C = Compliant, NC = Noncompliant, N/A = Not Applicable, and U = Unknown.

Table 17-3. Immediate Occupancy Basic Configuration Checklist

Status	Evaluation Statement	Tier 2 Reference	Commentary Reference
Very Low Seis			
Building Syste			
C NC N/A U	LOAD PATH: The structure contains a complete, well-defined load path, including structural elements and connections, that serves to transfer the inertial forces associated with the mass of all elements of the building to the foundation.	5.4.1.1	A.2.1.1
C NC N/A U	ADJACENT BUILDINGS: The clear distance between the building being evaluated and any adjacent building is greater than 0.5% of the height of the shorter building in low seismicity, 1.0% in moderate seismicity, and 3.0% in high seismicity.	5.4.1.2	A.2.1.2
C NC N/A U	MEZZANINES: Interior mezzanine levels are braced independently from the main structure or are anchored to the seismic-force-resisting elements of the main structure.	5.4.1.3	A.2.1.3
Building System	em—Building Configuration		
C NC N/A U	WEAK STORY: The sum of the shear strengths of the seismic-force-resisting system in any story in each direction is not less than 80% of the strength in the adjacent story above.	5.4.2.1	A.2.2.2
C NC N/A U	SOFT STORY: The stiffness of the seismic-force-resisting system in any story is not less than 70% of the seismic-force-resisting system stiffness in an adjacent story above or less than 80% of the average seismic-force-resisting system stiffness of the three stories above.	5.4.2.2	A.2.2.3
C NC N/A U	VERTICAL IRREGULARITIES: All vertical elements in the seismic- force-resisting system are continuous to the foundation.	5.4.2.3	A.2.2.4
C NC N/A U	GEOMETRY: There are no changes in the net horizontal dimension of the seismic-force-resisting system of more than 30% in a story relative to adjacent stories, excluding one-story penthouses and mezzanines.	5.4.2.4	A.2.2.5
C NC N/A U	MASS: There is no change in effective mass of more than 50% from one story to the next. Light roofs, penthouses, and mezzanines need not be considered.	5.4.2.5	A.2.2.6

Table 17-6. Collapse Prevention Structural Checklist for Building Type W2

Status	Evaluation Statement	Tier 2 Reference	Commentary Reference
Low and Mod	lerate Seismicity		
	e-Resisting System		
C NC N/A U	REDUNDANCY: The number of lines of shear walls in each principal direction is greater than or equal to 2.	5.5.1.1	A.3.2.1.1
C NCN/A U	SHEAR STRESS CHECK: The shear stress in the shear walls, calculated using the Quick Check procedure of Section 4.4.3.3, is less than the following values:	5.5.3.1.1	A.3.2.7.1
	Structural panel sheathing1,000 lb/ftDiagonal sheathing700 lb/ftStraight sheathing100 lb/ftAll other conditions100 lb/ft		
C NC 🕅 U	STUCCO (EXTERIOR PLASTER) SHEAR WALLS: Multi-story buildings do not rely on exterior stucco walls as the primary seismic-force-resisting system.	5.5.3.6.1	A.3.2.7.2
C NC 🕅 U	GYPSUM WALLBOARD OR PLASTER SHEAR WALLS: Interior plaster or gypsum wallboard is not used for shear walls on buildings more than one story high with the exception of the uppermost level of a multi-story building.	5.5.3.6.1	A.3.2.7.3
C NCN/A U	NARROW WOOD SHEAR WALLS: Narrow wood shear walls with an aspect ratio greater than 2-to-1 are not used to resist seismic forces.	5.5.3.6.1	A.3.2.7.4
C NC 🗤 U	WALLS CONNECTED THROUGH FLOORS: Shear walls have an interconnection between stories to transfer overturning and shear forces through the floor.	5.5.3.6.2	A.3.2.7.5
C NC 🗤 U	HILLSIDE SITE: For structures that are taller on at least one side by more than one-half story because of a sloping site, all shear walls on the downhill slope have an aspect ratio less than 1-to-1.	5.5.3.6.3	A.3.2.7.6
C NC 🕡 U	CRIPPLE WALLS: Cripple walls below first-floor-level shear walls are braced to the foundation with wood structural panels.	5.5.3.6.4	A.3.2.7.7
C <mark>NC</mark> N/A U	OPENINGS: Walls with openings greater than 80% of the length are braced with wood structural panel shear walls with aspect ratios of not more than 1.5-to-1 or are supported by adjacent construction through positive ties capable of transferring the seismic forces.	5.5.3.6.5	A.3.2.7.8
Connections	·		
CNCN/A U	WOOD POSTS: There is a positive connection of wood posts to the foundation.	5.7.3.3	A.5.3.3
CNCN/AU	WOOD SILLS: All wood sills are bolted to the foundation.	5.7.3.3	A.5.3.4
CNCN/A U	GIRDER–COLUMN CONNECTION: There is a positive connection using plates, connection hardware, or straps between the girder and the column support.	5.7.4.1	A.5.4.1
High Seismic Connections	ity (Complete the Following Items in Addition to the Items for Low and Mode	rate Seismicit	y)
CNCN/A U	WOOD SILL BOLTS: Sill bolts are spaced at 6 ft (1.8 m) or less with acceptable edge and end distance provided for wood and concrete.	5.7.3.3	A.5.3.7
Diaphragms	DIAPHRAGM CONTINUITY: The diaphragms are not composed of split-level floors and do not have expansion joints.	5.6.1.1	A.4.1.1
CNC N/A U	ROOF CHORD CONTINUITY: All chord elements are continuous, regardless of changes in roof elevation.	5.6.1.1	A.4.1.3
C NC <mark>()/A</mark> U	DIAPHRAGM REINFORCEMENT AT OPENINGS: There is reinforcing around all diaphragm openings larger than 50% of the building width in either major plan dimension.	5.6.1.5	A.4.1.8
C <mark>NC</mark> N/A U	STRAIGHT SHEATHING: All straight-sheathed diaphragms have aspect ratios less than 2-to-1 in the direction being considered.	5.6.2	A.4.2.1
C NCN/A U	SPANS: All wood diaphragms with spans greater than 24 ft (7.3 m) consist of wood structural panels or diagonal sheathing.	5.6.2	A.4.2.2

Table 17-6 (Continued). Collapse Prevention Structural Checklist for Building Type W2

Status	Evaluation Statement	Tier 2 Reference	Commentary Reference
C <mark>NC</mark> N/A U	DIAGONALLY SHEATHED AND UNBLOCKED DIAPHRAGMS: All diagonally sheathed or unblocked wood structural panel diaphragms have horizontal spans less than 40 ft (12.2 m) and have aspect ratios less than or equal to 4-to-1.	5.6.2	A.4.2.3
CNC N/A U	OTHER DIAPHRAGMS: The diaphragms do not consist of a system other than wood, metal deck, concrete, or horizontal bracing.	5.6.5	A.4.7.1

Note: C = Compliant, NC = Noncompliant, N/A = Not Applicable, and U = Unknown.

Table 17-7. Immediate Occupancy Checklist for Building Type W2

Status	Evaluation Statement	Tier 2 Reference	Commentary Reference
Very Low Seis			
	e-Resisting System		
C NC N/A U	REDUNDANCY: The number of lines of shear walls in each principal direction is greater than or equal to 2.	5.5.1.1	A.3.2.1.1
C NC N/A U	SHEAR STRESS CHECK: The shear stress in the shear walls, calculated using the Quick Check procedure of Section 4.4.3.3, is less than the following values:	5.5.3.1.1	A.3.2.7.1
	Structural panel sheathing1,000 lb/ft (14.6 kN/m)Diagonal sheathing700 lb/ft (10.2 kN/m)Straight sheathing100 lb/ft (1.5 kN/m)All other conditions100 lb/ft (1.5 kN/m)		
C NC N/A U	STUCCO (EXTERIOR PLASTER) SHEAR WALLS: Multi-story buildings do not rely on exterior stucco walls as the primary seismic-force-resisting system.	5.5.3.6.1	A.3.2.7.2
C NC N/A U	GYPSUM WALLBOARD OR PLASTER SHEAR WALLS: Interior plaster or gypsum wallboard is not used for shear walls on buildings more than one story high with the exception of the uppermost level of a multi-story building.	5.5.3.6.1	A.3.2.7.3
C NC N/A U	NARROW WOOD SHEAR WALLS: Narrow wood shear walls with an aspect ratio greater than 2-to-1 are not used to resist seismic forces.	5.5.3.6.1	A.3.2.7.4
C NC N/A U	WALLS CONNECTED THROUGH FLOORS: Shear walls have an interconnection between stories to transfer overturning and shear forces through the floor.	5.5.3.6.2	A.3.2.7.5
C NC N/A U	HILLSIDE SITE: For structures that are taller on at least one side by more than one-half story because of a sloping site, all shear walls on the downhill slope have an aspect ratio less than 1-to-2.	5.5.3.6.3	A.3.2.7.6
C NC N/A U	CRIPPLE WALLS: Cripple walls below first-floor-level shear walls are braced to the foundation with wood structural panels.	5.5.3.6.4	A.3.2.7.7
C NC N/A U	OPENINGS: Walls with openings greater than 80% of the length are braced with wood structural panel shear walls with aspect ratios of not more than 1.5-to-1 or are supported by adjacent construction through positive ties capable of transferring the seismic forces.	5.5.3.6.5	A.3.2.7.8
C NC N/A U	HOLD-DOWN ANCHORS: All shear walls have hold-down anchors attached to the end studs constructed in accordance with acceptable construction practices.	5.5.3.6.6	A.3.2.7.9
Connections		6 7 0 0	
C NC N/A U	WOOD POSTS: There is a positive connection of wood posts to the foundation.	5.7.3.3	A.5.3.3
C NC N/A U C NC N/A U	WOOD SILLS: All wood sills are bolted to the foundation. GIRDER-COLUMN CONNECTION: There is a positive connection using plates, connection hardware, or straps between the girder and the column support.	5.7.3.3 5.7.4.1	A.5.3.4 A.5.4.1

WESTMORELAND CAMPUS PHASE 1 BUILDINGS C & D G-1294-19

Table 17-38. Nonstructural Checklist

Status	Evaluation Statement ^{a,b}	Tier 2 Reference	Commentary Reference
Life Safety Sy	vstems		
	HR—not required; LS—LMH; PR—LMH. FIRE SUPPRESSION PIPING: Fire suppression piping is anchored and braced in accordance with NFPA-13.	13.7.4	A.7.13.1
	HR—not required; LS—LMH; PR—LMH. FLEXIBLE COUPLINGS: Fire suppression piping has flexible couplings in accordance with NFPA-13.	13.7.4	A.7.13.2
	HR—not required; LS—LMH; PR—LMH. EMERGENCY POWER: Equipment used to power or control Life Safety systems is anchored or braced.	13.7.7	A.7.12.1
C NC (N/A) U	HR—not required; LS—LMH; PR—LMH. STAIR AND SMOKE DUCTS: Stair pressurization and smoke control ducts are braced and have flexible connections at seismic joints.	13.7.6	A.7.14.1
C NC NA U	HR—not required; LS—MH; PR—MH . SPRINKLER CEILING CLEARANCE: Penetrations through panelized ceilings for fire suppression devices provide clearances in accordance with NFPA-13.	13.7.4	A.7.13.3
C NC 🗤 U	HR—not required; LS—not required; PR—LMH . EMERGENCY LIGHTING: Emergency and egress lighting equipment is anchored or braced.	13.7.9	A.7.3.1
Hazardous Ma			
C NC (V/A)U	HR—LMH; LS—LMH; PR—LMH . HAZARDOUS MATERIAL EQUIPMENT: Equipment mounted on vibration isolators and containing hazardous material is equipped with restraints or snubbers.	13.7.1	A.7.12.2
C NC 🗤 U	HR—LMH; LS—LMH; PR—LMH. HAZARDOUS MATERIAL STORAGE: Breakable containers that hold hazardous material, including gas cylinders, are restrained by latched doors, shelf lips, wires, or other methods.	13.8.3	A.7.15.1
C <mark>NC</mark> N/A U	HR—MH; LS—MH; PR—MH . HAZARDOUS MATERIAL DISTRIBUTION: Piping or ductwork conveying hazardous materials is braced or otherwise protected from damage that would allow hazardous material release.	13.7.3 13.7.5	A.7.13.4
C <mark>NC</mark> N/A U	HR—MH; LS—MH; PR—MH. SHUTOFF VALVES: Piping containing hazardous material, including natural gas, has shutoff valves or other devices to limit spills or leaks.	13.7.3 13.7.5	A.7.13.3
CNCN/A U	HR—LMH; LS—LMH; PR—LMH . FLEXIBLE COUPLINGS: Hazardous material ductwork and piping, including natural gas piping, have flexible couplings.	13.7.3 13.7.5	A.7.15.4
C NC 🗤 U	HR—MH; LS—MH; PR—MH . PIPING OR DUCTS CROSSING SEISMIC JOINTS: Piping or ductwork carrying hazardous material that either crosses seismic joints or isolation planes or is connected to independent structures has couplings or other details to accommodate the relative seismic displacements.	13.7.3 13.7.5 13.7.6	A.7.13.6
Partitions C NC NA U	HR—LMH; LS—LMH; PR—LMH . UNREINFORCED MASONRY: Unreinforced masonry or hollow-clay tile partitions are braced at a spacing of at most 10 ft (3.0 m) in Low or Moderate Seismicity, or at most 6 ft (1.8 m) in High Seismicity.	13.6.2	A.7.1.1
C NC 🗤 U	HR—LMH; LS—LMH; PR—LMH. HEAVY PARTITIONS SUPPORTED BY CEILINGS: The tops of masonry or hollow-clay tile partitions are not laterally supported by an integrated ceiling system.	13.6.2	A.7.2.1
C NC 🕡 U	HR—not required; LS—MH; PR—MH. DRIFT: Rigid cementitious partitions are detailed to accommodate the following drift ratios: in steel moment frame, concrete moment frame, and wood frame buildings, 0.02; in other buildings, 0.005.	13.6.2	A.7.1.2
C NC 🗤 U	HR—not required; LS—not required; PR—MH. LIGHT PARTITIONS SUPPORTED BY CEILINGS: The tops of gypsum board partitions are not laterally supported by an integrated ceiling system.	13.6.2	A.7.2.1
C NC 🗤 U	HR—not required; LS—not required; PR—MH. STRUCTURAL SEPARATIONS: Partitions that cross structural separations have seismic or control joints.	13.6.2	A.7.1.3

Table 17-38 (Continued). Nonstructural Checklist

Status	Evaluation Statement ^{a,b}	Tier 2 Reference	Commentary Reference
CNCN/A U Ceilings	HR—not required; LS—not required; PR—MH . TOPS: The tops of ceiling-high framed or panelized partitions have lateral bracing to the structure at a spacing equal to or less than 6 ft (1.8 m).	13.6.2	A.7.1.4
	HR—H; LS—MH; PR—LMH . SUSPENDED LATH AND PLASTER: Suspended lath and plaster ceilings have attachments that resist seismic forces for every 12 ft ² (1.1 m ²) of area.	13.6.4	A.7.2.3
C NC 🗤 U	HR—not required; LS—MH; PR—LMH . SUSPENDED GYPSUM BOARD: Suspended gypsum board ceilings have attachments that resist seismic forces for every 12 ft ² (1.1 m ²) of area.	13.6.4	A.7.2.3
CNC N/A U	HR —not required; LS —not required; PR —MH. INTEGRATED CEILINGS: Integrated suspended ceilings with continuous areas greater than 144 ft ² (13.4 m ²) and ceilings of smaller areas that are not surrounded by restraining partitions are laterally restrained at a spacing no greater than 12 ft (3.6 m) with members attached to the structure above. Each restraint location has a minimum of four diagonal wires and compression struts, or diagonal members capable of resisting compression.	13.6.4	A.7.2.2
CNC N/A U	HR —not required; LS —not required; PR —MH. EDGE CLEARANCE: The free edges of integrated suspended ceilings with continuous areas greater than 144 ft ² (13.4 m ²) have clearances from the enclosing wall or partition of at least the following: in Moderate Seismicity, 1/2 in. (13 mm); in High Seismicity, 3/4 in. (19 mm).	13.6.4	A.7.2.4
C NC 😡 U	HR—not required; LS—not required; PR—MH. CONTINUITY ACROSS STRUCTURE JOINTS: The ceiling system does not cross any seismic joint and is not attached to multiple independent structures.	13.6.4	A.7.2.5
CNC N/A U	HR—not required; LS—not required; PR—H . EDGE SUPPORT: The free edges of integrated suspended ceilings with continuous areas greater than 144 ft ² (13.4 m ²) are supported by closure angles or channels not less than 2 in. (51 mm) wide.	13.6.4	A.7.2.6
	HR—not required; LS—not required; PR—H . SEISMIC JOINTS: Acoustical tile or lay-in panel ceilings have seismic separation joints such that each continuous portion of the ceiling is no more than 2,500 ft ² (232.3 m ²) and has a ratio of long-to-short dimension no more than 4-to-1.	13.6.4	A.7.2.7
Light Fixtures CNC N/A U	HR—not required; LS—MH; PR—MH. INDEPENDENT SUPPORT: Light fixtures that weigh more per square foot than the ceiling they penetrate are supported independent of the grid ceiling suspension system by a minimum of two wires at diagonally opposite corners of each fixture.	13.6.4 13.7.9	A.7.3.2
	HR —not required; LS —not required; PR — H . PENDANT SUPPORTS: Light fixtures on pendant supports are attached at a spacing equal to or less than 6 ft. Unbraced suspended fixtures are free to allow a 360-degree range of motion at an angle not less than 45 degrees from horizontal without contacting adjacent components. Alternatively, if rigidly supported and/or braced, they are free to move with the structure to which they are attached without damaging adjoining components. Additionally, the connection to the structure is capable of accommodating the movement without failure.	13.7.9	A.7.3.3
CNC N/A U	HR—not required; LS—not required; PR—H. LENS COVERS: Lens covers on light fixtures are attached with safety devices.	13.7.9	A .7.3.4
	 HR—MH; LS—MH; PR—MH. CLADDING ANCHORS: Cladding components weighing more than 10 lb/ft² (0.48 kN/m²) are mechanically anchored to the structure at a spacing equal to or less than the following: for Life Safety in Moderate Seismicity, 6 ft (1.8 m); for Life Safety in High Seismicity and for Position Retention in any seismicity, 4 ft (1.2 m) 	13.6.1	A.7.4.1

Table 17-38 (Continued). Nonstructural Checklist

Status	Evaluation Statement ^{a,b}	Tier 2 Reference	Commentary Reference
C NC WA U	HR—not required; LS—MH; PR—MH. CLADDING ISOLATION: For steel or concrete moment-frame buildings, panel connections are detailed to accommodate a story drift ratio by the use of rods attached to framing with oversize holes or slotted holes of at least the following: for Life Safety in Moderate Seismicity, 0.01; for Life Safety in High Seismicity and for Position Retention in any seismicity, 0.02, and the rods have a length-to-diameter ratio of 4.0 or less.	13.6.1	A.7.4.3
C NC 🕪 U	HR—MH; LS—MH; PR—MH . MULTI-STORY PANELS: For multi-story panels attached at more than one floor level, panel connections are detailed to accommodate a story drift ratio by the use of rods attached to framing with oversize holes or slotted holes of at least the following: for Life Safety in Moderate Seismicity, 0.01; for Life Safety in High Seismicity and for Position Retention in any seismicity, 0.02, and the rods have a length-to-diameter ratio of 4.0 or less.	13.6.1	A.7.4.4
C NC WA U	HR—not required; LS—MH; PR—MH. THREADED RODS: Threaded rods for panel connections detailed to accommodate drift by bending of the rod have a length-to-diameter ratio greater than 0.06 times the story height in inches for Life Safety in Moderate Seismicity and 0.12 times the story height in inches for Life Safety in High Seismicity and Position Retention in any seismicity.	13.6.1	A.7.4.9
C NC 🕡 U	HR—MH; LS—MH; PR—MH . PANEL CONNECTIONS: Cladding panels are anchored out of plane with a minimum number of connections for each wall panel, as follows: for Life Safety in Moderate Seismicity, 2 connections; for Life Safety in High Seismicity and for Position Retention in any seismicity, 4 connections.	13.6.1.4	A.7.4.5
C NC 😡 U	HR—MH; LS—MH; PR—MH . BEARING CONNECTIONS: Where bearing connections are used, there is a minimum of two bearing connections for each cladding panel.	13.6.1.4	A.7.4.6
	HR—MH; LS—MH; PR—MH. INSERTS: Where concrete cladding components use inserts, the inserts have positive anchorage or are anchored to reinforcing steel.	13.6.1.4	A.7.4.7
C NC WA U	HR—not required; LS—MH; PR—MH . OVERHEAD GLAZING: Glazing panes of any size in curtain walls and individual interior or exterior panes more than 16 ft ² (1.5 m ²) in area are laminated annealed or laminated heat-strengthened glass and are detailed to remain in the frame when cracked.	13.6.1.5	A.7.4.8
Masonry Vene CNCN/A U	 HR—not required; LS—LMH; PR—LMH. TIES: Masonry veneer is connected to the backup with corrosion-resistant ties. There is a minimum of one tie for every 2-2/3 ft² (0.25 m²), and the ties have spacing no greater than the following: for Life Safety in Low or Moderate Seismicity, 36 in. (914 mm); for Life Safety in High Seismicity and for Position Retention in any seismicity, 24 in. (610 mm). 	13.6.1.2	A.7.5.1
C NC 🕅 U	HR—not required; LS—LMH; PR—LMH . SHELF ANGLES: Masonry veneer is supported by shelf angles or other elements at each floor above the ground floor.	13.6.1.2	A.7.5.2
C NCN/A U	HR—not required; LS—LMH; PR—LMH. WEAKENED PLANES: Masonry veneer is anchored to the backup adjacent to weakened planes, such as at the locations of flashing.	13.6.1.2	A.7.5.3
CNC N/A U	HR—LMH; LS—LMH; PR—LMH. UNREINFORCED MASONRY BACKUP: There is no unreinforced masonry backup.	13.6.1.1 13.6.1.2	A.7.7.2
C NC 🕅 U	HR—not required; LS—MH; PR—MH. STUD TRACKS: For veneer with cold- formed steel stud backup, stud tracks are fastened to the structure at a spacing equal to or less than 24 in. (610 mm) on center.	13.6.1.1 13.6.1.2	A.7.6.1

Table 17-38 (Continued)	Nonstructural Checklist
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Status	Evaluation Statement ^{a,b}	Tier 2 Reference	Commentary Reference
C NC 🕪 U	HR—not required; LS—MH; PR—MH . ANCHORAGE: For veneer with concrete block or masonry backup, the backup is positively anchored to the structure at a horizontal spacing equal to or less than 4 ft along the floors and roof.	13.6.1.1 13.6.1.2	A.7.7.1
C <mark>NC</mark> N/A U	HR—not required; LS—not required; PR—MH . WEEP HOLES: In veneer anchored to stud walls, the veneer has functioning weep holes and base flashing.	13.6.1.2	A.7.5.6
C NC 🕡 U	HR—not required; LS—not required; PR—MH. OPENINGS: For veneer with cold-formed-steel stud backup, steel studs frame window and door openings.	13.6.1.1 13.6.1.2	A.7.6.2
Parapets, Cor C NC N/A U	nices, Ornamentation, and Appendages HR—LMH; LS—LMH; PR—LMH. URM PARAPETS OR CORNICES: Laterally	13.6.5	A.7.8.1
Ŭ	unsupported unreinforced masonry parapets or cornices have height-to- thickness ratios no greater than the following: for Life Safety in Low or Moderate Seismicity, 2.5; for Life Safety in High Seismicity and for Position Retention in any seismicity, 1.5.		
C NCN/A U	HR—not required; LS—LMH; PR—LMH. CANOPIES: Canopies at building exits are anchored to the structure at a spacing no greater than the following: for Life Safety in Low or Moderate Seismicity, 10 ft (3.0 m); for Life Safety in High Seismicity and for Position Retention in any seismicity, 6 ft (1.8 m).	13.6.6	A.7.8.2
	HR—H ; LS—MH ; PR—LMH . CONCRETE PARAPETS: Concrete parapets with height-to-thickness ratios greater than 2.5 have vertical reinforcement.	13.6.5	A.7.8.3
C NC 🕡 U	 HR—MH; LS—MH; PR—LMH. APPENDAGES: Cornices, parapets, signs, and other ornamentation or appendages that extend above the highest point of anchorage to the structure or cantilever from components are reinforced and anchored to the structural system at a spacing equal to or less than 6 ft (1.8 m). This evaluation statement item does not apply to parapets or cornices covered by other evaluation statements. 	13.6.6	A.7.8.4
Masonry Chin		10.07	
C NC (N/A) U	HR—LMH; LS—LMH; PR—LMH. URM CHIMNEYS: Unreinforced masonry chimneys extend above the roof surface no more than the following: for Life Safety in Low or Moderate Seismicity, 3 times the least dimension of the chimney; for Life Safety in High Seismicity and for Position Retention in any seismicity, 2 times the least dimension of the chimney.	13.6.7	A.7.9.1
	HR—LMH; LS—LMH; PR—LMH . ANCHORAGE: Masonry chimneys are anchored at each floor level, at the topmost ceiling level, and at the roof.	13.6.7	A.7.9.2
Stairs C NC N/A U	HD not required, I.C. I.MH, DD I.MH, STAID ENCLOSUBES, Hollow day	13.6.2	A.7.10.1
	HR—not required; LS—LMH; PR—LMH. STAIR ENCLOSURES: Hollow-clay tile or unreinforced masonry walls around stair enclosures are restrained out of plane and have height-to-thickness ratios not greater than the following: for Life Safety in Low or Moderate Seismicity, 15-to-1; for Life Safety in High Seismicity and for Position Retention in any seismicity, 12-to-1.	13.6.8	A.7.10.1
C NC NA U	HR—not required; LS—LMH; PR—LMH. STAIR DETAILS: The connection between the stairs and the structure does not rely on post-installed anchors in concrete or masonry, and the stair details are capable of accommodating the drift calculated using the Quick Check procedure of Section 4.4.3.1 for moment-frame structures or 0.5 in. for all other structures without including any lateral stiffness contribution from the stairs.	13.6.8	A.7.10.2
C NC N/A U	HR—LMH; LS—MH; PR—MH. INDUSTRIAL STORAGE RACKS: Industrial	13.8.1	A.7.11.1
Ŭ	storage racks or pallet racks more than 12 ft high meet the requirements of ANSI/RMI MH 16.1 as modified by ASCE 7, Chapter 15.		

WESTMORELAND CAMPUS PHASE 1 BUILDINGS C & D G-1294-19

Table 17-38 (Continued). Nonstructural Checklist

Status	Evaluation Statement ^{a,b}	Tier 2 Reference	Commentary Reference
CNCN/A U	HR—not required; LS—H; PR—MH . TALL NARROW CONTENTS: Contents more than 6 ft (1.8 m) high with a height-to-depth or height-to-width ratio greater than 3-to-1 are anchored to the structure or to each other.	13.8.2	A.7.11.2
CNCN/A U	HR —not required; LS—H; PR—H. FALL-PRONE CONTENTS: Equipment, stored items, or other contents weighing more than 20 lb (9.1 kg) whose center of mass is more than 4 ft (1.2 m) above the adjacent floor level are braced or otherwise restrained.	13.8.2	A.7.11.3
	HR—not required; LS—not required; PR—MH. ACCESS FLOORS: Access floors more than 9 in. (229 mm) high are braced.	13.6.10	A.7.11.4
C NC (VA)U	HR—not required; LS—not required; PR—MH . EQUIPMENT ON ACCESS FLOORS: Equipment and other contents supported by access floor systems are anchored or braced to the structure independent of the access floor.	13.7.7 13.6.10	A.7.11.5
C NC MA U	 HR—not required; LS—not required; PR—H. SUSPENDED CONTENTS: Items suspended without lateral bracing are free to swing from or move with the structure from which they are suspended without damaging themselves or adjoining components. hd Electrical Equipment 	13.8.2	A.7.11.6
C NCN/A U	HR—not required; LS—H; PR—H. FALL-PRONE EQUIPMENT: Equipment	13.7.1	A.7.12.4
	weighing more than 20 lb (9.1 kg) whose center of mass is more than 4 ft (1.2 m) above the adjacent floor level, and which is not in-line equipment, is braced.	13.7.7	A.T. 12.4
C NC MA U	HR—not required; LS—H; PR—H. IN-LINE EQUIPMENT: Equipment installed in line with a duct or piping system, with an operating weight more than 75 lb (34.0 kg), is supported and laterally braced independent of the duct or piping system.	13.7.1	A.7.12.5
CNCN/A U	HR—not required; LS—H; PR—MH . TALL NARROW EQUIPMENT: Equipment more than 6 ft (1.8 m) high with a height-to-depth or height-to-width ratio greater than 3-to-1 is anchored to the floor slab or adjacent structural walls.	13.7.1 13.7.7	A.7.12.6
C NC 🕅 U	HR—not required; LS—not required; PR—MH. MECHANICAL DOORS: Mechanically operated doors are detailed to operate at a story drift ratio of 0.01.	13.6.9	A.7.12.7
C NC 🕅 U	HR—not required; LS—not required; PR—H . SUSPENDED EQUIPMENT: Equipment suspended without lateral bracing is free to swing from or move with the structure from which it is suspended without damaging itself or adjoining components.	13.7.1 13.7.7	A.7.12.8
	HR —not required; LS —not required; PR —H. VIBRATION ISOLATORS: Equipment mounted on vibration isolators is equipped with horizontal restraints or snubbers and with vertical restraints to resist overturning.	13.7.1	A.7.12.9
C <mark>NC</mark> N/A U	HR—not required; LS—not required; PR—H. HEAVY EQUIPMENT: Floor- supported or platform-supported equipment weighing more than 400 lb (181.4 kg) is anchored to the structure.	13.7.1 13.7.7	A.7.12.10
CNC N/A U	HR—not required; LS—not required; PR—H. ELECTRICAL EQUIPMENT: Electrical equipment is laterally braced to the structure.	13.7.7	A.7.12.11
C NC NA U	HR —not required; LS —not required; PR —H. CONDUIT COUPLINGS: Conduit greater than 2.5 in. (64 mm) trade size that is attached to panels, cabinets, or other equipment and is subject to relative seismic displacement has flexible couplings or connections.	13.7.8	A.7.12.12
Piping C NCN/A U	HR—not required; LS—not required; PR—H. FLEXIBLE COUPLINGS: Fluid and gas piping has flexible couplings.	13.7.3 13.7.5	A.7.13.2

continues

WESTMORELAND CAMPUS PHASE 1 **BUILDINGS C & D** G-1294-19

Table 17-38 (Continued). Nonstructural Checklist

Status	Evaluation Statement ^{a,b}	Tier 2 Reference	Commentary Reference
C <mark>NC</mark> N/A U	HR—not required; LS—not required; PR—H . FLUID AND GAS PIPING: Fluid and gas piping is anchored and braced to the structure to limit spills or leaks.	13.7.3 13.7.5	A.7.13.4
CNCN/A U	HR—not required; LS—not required; PR—H. C-CLAMPS: One-sided C-clamps that support piping larger than 2.5 in. (64 mm) in diameter are restrained.	13.7.3 13.7.5	A.7.13.5
C NC 🗤 U	HR—not required; LS—not required; PR—H. PIPING CROSSING SEISMIC JOINTS: Piping that crosses seismic joints or isolation planes or is connected to independent structures has couplings or other details to accommodate the relative seismic displacements.	13.7.3 13.7.5	A.7.13.6
Ducts CNC N/A U	HR—not required; LS—not required; PR—H . DUCT BRACING: Rectangular ductwork larger than 6 ft ² (0.56 m ²) in cross-sectional area and round ducts larger than 28 in. (711 mm) in diameter are braced. The maximum spacing of transverse bracing does not exceed 30 ft (9.2 m). The maximum spacing of longitudinal bracing does not exceed 60 ft (18.3 m).	13.7.6	A.7.14.2
CNC N/A U	HR—not required; LS—not required; PR—H. DUCT SUPPORT: Ducts are not supported by piping or electrical conduit.	13.7.6	A.7.14.3
C NC 🕅 U	HR—not required; LS—not required; PR—H. DUCTS CROSSING SEISMIC JOINTS: Ducts that cross seismic joints or isolation planes or are connected to independent structures have couplings or other details to accommodate the relative seismic displacements.	13.7.6	A.7.14.4
Elevators			
	HR—not required; LS—H; PR—H. RETAINER GUARDS: Sheaves and drums have cable retainer guards.	13.7.11	A.7.16.1
	HR—not required; LS—H; PR—H. RETAINER PLATE: A retainer plate is present at the top and bottom of both car and counterweight.	13.7.11	A.7.16.2
C NC (N/A) U	HR—not required; LS—not required; PR—H . ELEVATOR EQUIPMENT: Equipment, piping, and other components that are part of the elevator system are anchored.	13.7.11	A.7.16.3
C NC MAU	HR—not required; LS—not required; PR—H. SEISMIC SWITCH: Elevators capable of operating at speeds of 150 ft/min (0.30 m/min) or faster are equipped with seismic switches that meet the requirements of ASME A17.1 or have trigger levels set to 20% of the acceleration of gravity at the base of the structure and 50% of the acceleration of gravity in other locations.	13.7.11	A.7.16.4
C NC 🕅 U	HR—not required; LS—not required; PR—H. SHAFT WALLS: Elevator shaft walls are anchored and reinforced to prevent toppling into the shaft during strong shaking.	13.7.11	A.7.16.5
C NC 🕪 U	HR—not required; LS—not required; PR—H . COUNTERWEIGHT RAILS: All counterweight rails and divider beams are sized in accordance with ASME A17.1.	13.7.11	A.7.16.6
C NC 🕪 U	HR—not required; LS—not required; PR—H . BRACKETS: The brackets that tie the car rails and the counterweight rail to the structure are sized in accordance with ASME A17.1.	13.7.11	A.7.16.7
C NC 🕅 U	HR—not required; LS—not required; PR—H . SPREADER BRACKET: Spreader brackets are not used to resist seismic forces.	13.7.11	A.7.16.8
C NC N/A U	HR—not required; LS—not required; PR—H. GO-SLOW ELEVATORS: The building has a go-slow elevator system.	13.7.11	A.7.16.9

Note: C = Compliant, NC = Noncompliant, N/A = Not Applicable, and U = Unknown. ^a Performance Level: HR = Hazards Reduced, LS = Life Safety, and PR = Position Retention. ^b Level of Seismicity: L = Low, M = Moderate, and H = High.

Liquefaction Map



Esri, HERE, Garmin, (c) OpenStreetMap contributors, and the GIS user





Esri, HERE, Garmin, (c) OpenStreetMap contributors, and the GIS user

Active Faults Map



Esri, HERE, Garmin, (c) OpenStreetMap contributors, and the GIS user

0.03

0.01

0

—— Active Faults



OSHPD

1717 City View St, Eugene, OR 97402, USA

Latitude, Longitude: 44.04088, -123.12713489999999

	The Little French School, Inc School, Inc W 18th Ave W 18th Ave Willamette Christian Center	W 18th Ave Grant st Map data ©2020
Date	1/7/2020, 11:45:31 AM	
Design Code Referen	ASCE41-17	
Custom Probability Site Class	D - Stiff Soil	
Sile Class		
Туре	Description	Value
Hazard Level		BSE-2N
SS	spectral response (0.2 s)	0.721
S ₁	spectral response (1.0 s)	0.411
S _{XS}	site-modified spectral response (0.2 s)	0.882
S _{X1}	site-modified spectral response (1.0 s)	0.776
Fa	site amplification factor (0.2 s)	1.223
F _v	site amplification factor (1.0 s)	1.889
ssuh	max direction uniform hazard (0.2 s)	0.827
crs	coefficient of risk (0.2 s)	0.871
ssrt	risk-targeted hazard (0.2 s)	0.721
ssd	deterministic hazard (0.2 s)	1.5
s1uh	max direction uniform hazard (1.0 s)	0.478
cr1	coefficient of risk (1.0 s)	0.859
s1rt	risk-targeted hazard (1.0 s)	0.411
s1d	deterministic hazard (1.0 s)	0.68
_	–	
Type Hazard Level	Description	Value BSE-1N
S _{XS}	site-modified spectral response (0.2 s)	0.588
	site-modified spectral response (0.2 s)	
S _{X1}	site-mounieu spectral response (1.0 s)	0.517

T-Sub-L

Туре	Description	Value
Hazard Level		BSE-2E
SS	spectral response (0.2 s)	0.493
S ₁	spectral response (1.0 s)	0.279
S _{XS}	site-modified spectral response (0.2 s)	0.693
S _{X1}	site-modified spectral response (1.0 s)	0.569
f _a	site amplification factor (0.2 s)	1.406
f _v	site amplification factor (1.0 s)	2.043

Туре	Description	Value
Hazard Level		BSE-1E
S _S	spectral response (0.2 s)	0.121
S ₁	spectral response (1.0 s)	0.057
S _{XS}	site-modified spectral response (0.2 s)	0.193
S _{X1}	site-modified spectral response (1.0 s)	0.137
F _a	site amplification factor (0.2 s)	1.6
F _v	site amplification factor (1.0 s)	2.4
Туре	Description	Value
Hazard Level		TL Data

DISCLAIMER

Long-period transition period in seconds

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16



Pali Consulting

January 16, 2020

MEMORANDUM

Westmoreland Elementary School Preliminary Geologic Hazards Evaluation ZCS Engineering and Architecture Attention Mr. Andre Latyk Pali Consulting Project #013-20-048



1.0 INTRODUCTION

Pali Consulting, Inc. (Pali Consulting) presents this evaluation of geologic hazards at Westmoreland Elementary School in Eugene, Oregon. ZCS Engineering and Architecture (ZCS) is performing seismic rehabilitation design for the school. As part of their work, ZCS requested that we complete a preliminary evaluation of geologic hazards present at the site, in particular those related to earthquakes. The evaluation is to determine if geotechnical hazards resulting from earthquake shaking are likely to be present at the site for consideration in their grant application for the seismic upgrade funding. Specific geotechnical design is not provided in this memorandum and no subsurface explorations were completed. The site is located at 1717 City View Street in Eugene, Oregon. Our work was completed in general accordance with our master service agreement with ZCS Engineering and Architecture, dated September 27, 2018, and Task Order 42.

2.0 BACKGROUND

We reviewed the geology of the site and mapped seismic hazards, including earthquake induced landsliding, liquefaction, and active faults. A summary of our review follows.

2.1 GEOLOGY

The geology in the area is mapped on the Oregon Department of Geology and Mineral Industries' (DOGAMI) website (<u>https://gis.dogami.oregon.gov/maps/geologicmap/#</u>, accessed January 2020). The website maps the site on the boundary between Quaternary Surficial Deposits to the north and east, and sandstone to the west and south. The surficial deposits are described as unconsolidated mixed-grained sediments that can be derived from a number of sources, including alluvium, colluvium, glacial, landslide,



colian, outburst flood, and many others. The sandstone is described as Eocene to Oligocene marine sedimentary rocks of the Eugene Formation. The units are more specifically described in DOGAMI Open File Report O-10-03 Geologic Map of the Southern Willamette Valley, Benton, Lane, Linn, Marion, and Polk Counties, Oregon (McClaughry, Wiley, Ferns, and Madin, 2010). The alluvial deposits (Ha) are described as unconsolidated gravel, sand, silt and clay deposited in active stream channels and on adjoining flood plains, and the unit is reported to be up to 50 feet thick. To the west and south, siliciclastic marine sedimentary rocks (Tms) are further described as micaceous and arkosic sandstone, siltstone and minor volcaniclastic conglomerate. It is reported that this unit may be susceptible to landslides where bedding planes are moderately to steeply dipping. These types of sedimentary rocks likely underlie the Quaternary deposits within the school area, but at an unknown depth.

We reviewed well logs near the site on the Oregon Water Resources Department website (https://apps.wrd.state.or.us/apps/gw/well_log/, accessed January 2020). Several well logs were reviewed in proximity to the school site and generally within the same terrace landform. These well logs had similar profiles, generally consisting of clay or silt with sand and gravel overlying sedimentary bedrock at various depths to the depths explored, which were up to 200 feet below the ground surface (bgs). The sedimentary bedrock was described as blue sandstone or claystone and generally noted as shallow as 30 feet bgs in two logs to as deep as 80 to 100 feet bgs in two other logs. One log described hard basalt at 23 feet bgs rather than sedimentary rock, although this is doubtful. All well logs reported relatively shallow static water levels of between about 5 to 25 feet bgs, although many logs did not indicate a static water level.

2.2 LIDAR, TOPOGRAPHY AND LANDFORMS

We interpreted digital information related to landforms at the site, using LiDAR and topographic maps available on the DOGAMI website (https://gis.dogami.oregon.gov/maps/hazvu/, accessed January 2020) and on Google Earth TM. These sources show the school is located on a wide and relatively flat alluvial terrace at the south end of the Willamette Valley. The terrace surface is generally planar, with little relief and approximately 7 miles wide northeast/southwest at the school location, widening to the north. The terrace is being incised by streams and rivers locally, most notably Amazon Creek and the Willamette and McKenzie Rivers, which are approximately 0.25, 2 and 5.5 miles to the northeast of the school, respectively. The ground surface at the site slopes gently downward to the northeast toward Amazon Creek, and moderately steep uphill to several unnamed ridges and hilltops about a quarter mile to the southwest.

2.3 OTHER REPORTS AND DOCUMENTS

We were not able to locate records of existing geotechnical reports or other sources of information.

2.4 GEOLOGIC HAZARDS

Geologic hazards were accessed and reviewed on the DOGAMI HazVu website (<u>https://gis.dogami.oregon.gov/maps/hazvu/</u>, accessed January 2020). We found the following regarding hazards mapped at the site:

- Subject to strong to very strong shaking from Cascadia and local earthquakes.
- No landslides are mapped in areas where buildings are located, which also have a low to moderate landslide hazard.
- Soil liquefaction hazard is mapped as none to moderate.
- Not within the FEMA 100-year floodplain.

January 16, 2020



- Not within a tsunami inundation zone.
- Nearest active faults are approximately 25 miles to the southeast of the site.

3.0 CONCLUSIONS

The site is located within an area mapped as subject to strong to very strong shaking from Cascadia and Local earthquake sources. The site is also mapped with a moderate liquefaction hazard on the east side of the school and a low to moderate landslide hazard. Other geologic hazards are low, not mapped, or likely not present at the site.

Based on our review of the site landforms (geomorphology), geology, and well logs, we conclude the following:

- Earthquake shaking is present at the site as mapped,
- Soil liquefaction hazard is probably moderate, and
- Landslide hazard is probably low.

Earthquake shaking will be addressed by code-level design for the facility. Soil liquefaction and landslide hazards are described in more detail below.

3.1 SOIL LIQUEFACTION

Soil liquefaction can result in post-seismic settlement, soil strength loss, and lateral spread. We note the following site-specific factors related to soil liquefaction at this site:

- Groundwater Depth. Nearby well logs show static groundwater depths in the area at between 5 to 25 feet bgs. Below a few feet of topsoil, soils appear to consist of clays and silts with some sand and gravel. The site is on an alluvial terrace of the Willamette River and nearby Amazon Creek, which is incised only a few feet into the terrace. Groundwater at the school could, therefore, be relatively shallow during much of the year. Soils below groundwater level could be subject to liquefaction.
- Soil Composition. Soils in nearby well logs are variable, described as gravel, sand, silt and clay which appears interbedded, typical of alluvial terraces. The majority of well logs documents the soils as predominately clay. From the well log descriptions, liquefaction of the sands and gravels appears likely and may extend to many tens of feet bgs. Potential liquefaction of clays is less likely.
- Soil Age. Aged soils are less prone to liquefaction than young soils. Holocene age soils, those formed or deposited in the last 10,000 or so years, are considered to be liquefiable, while older Pleistocene age soils (about 10,000 to 2,000,000 years old) are less likely to liquefy. The soils are identified as mostly Holocene with some Late Pleistocene alluvium. This suggests site soils are likely to liquefy.

Based on our review and analyses it is our opinion that site soils have a moderate potential to experience liquefaction under strong earthquake shaking. This is based on the presence of silt, sand and gravel which are potentially liquefiable, likely saturation of soils to between 5 and 25 feet bgs, and the mostly Holocene



geologic age of the soils. If liquefaction occurs, we expect that seismic-induced settlement will occur. The magnitude of settlement depends largely on the thickness of liquefiable soils and their composition. The potential for local bearing capacity failure will depend on the depth to the top of the liquefiable soils.

Typically, about 10 feet of non-liquefiable soil below footing subgrade greatly reduces the bearing capacity failure hazard. Sufficient information to estimate settlement magnitude is not available. Two well logs showed sands and gravels to around 30 feet bgs before encountering bedrock, but other logs showed bedrock around 80 to 100 feet bgs, so the extent of such soils could not be verified. Many well logs showed interbedded silts with the gravels and sands which would act to reduce settlement compared to only sands and gravels, while some logs showed strictly clay which would not liquify. Based on the information available, seismic-induced differential settlements could exceed design thresholds for the immediate occupancy performance level and possibly for the limited life safety performance level as well. Local bearing failure is less likely and may be reduced by overlying non-liquefiable soils but is still possible.

3.2 LANDSLIDE HAZARD

The area of moderate landslide hazard near the school is not associated with an obvious physical feature in the LiDAR data and is most likely due to geologic mapping of the sandstone/alluvium contact. Such features would not pose a significant landslide hazard to the school, as the slope gradient at the site is fairly gentle, so we interpret landslide hazards to still be low.

3.3 FOUNDATIONS

Because of the potential for soil liquefaction, foundation design should consider and address this hazard. Choosing an appropriate foundation system at this point is not possible, as the depth to bearing material is unknown. Based on one boring log, the alluvial deposits extend to 100 feet or more bgs. If this depth is representative of the site, underpinning or pile-supporting the school structure may not be feasible. However, most well logs indicated alluvium is shallow, extending only to around 30 feet bgs. Underpinning will be the most likely measure to mitigate for seismic-induced settlement in this case and which would also address local bearing capacity failure. The depth of liquefiable soils and any underlying bearing layer are not known and will affect the feasibility and depth of underpinning elements.

If liquefiable soils are too deep to make underpinning possible, the most likely mitigation would be to connect new and existing footings with grade beams and strengthen structural connections to reduce differential settlements and prevent collapse. It is unlikely this would be able to achieve the immediate occupancy operational level but could possibly achieve the limited life safety operational level.

Based on the data reviewed, underpinning to a depth of 30 to 50 feet bgs appears to be the most likely and feasible foundation mitigation design.

3.4 Additional Geotechnical Explorations

Subsurface explorations are recommended to confirm site conditions, confirm our interpretation of geologic hazards, and to provide final geotechnical design parameters.



4.0 CLOSING AND LIMITATIONS

This report is based on available public information and our geotechnical experience. No subsurface explorations were completed. The opinions and recommendations contained within this report are, therefore, based on evaluation of very limited information and should not be construed as a warranty or guarantee of site conditions or performance. Soil conditions can differ from those portrayed in the sources we reviewed, as well as during different seasons, from earth processes, from storms, or other factors that occur after our work has been completed.

Within the limitations of scope, schedule, and budget, our services have been executed in accordance with the standard of care in this area at the time this report was prepared. No warranty or other conditions, express or implied, should be understood.

We appreciate the opportunity to provide this information for you. Please contact us if we can be of further assistance or if you have any questions.

Document ID: 013-19-048WestmorelandESHazardMemo



Appendix C: Construction Cost Estimate Worksheets

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Description (Ref. Semile Evaluation Report Sec. 4.9) Quantity Units Unit Price Construction its General Conditions Preconstruction Services 2% % 130, \$ 140, 130, \$ 140, 130, \$ 140, 130, \$ 140, 130, \$ 140, 130, \$ 180, 1							
Description If it estantion Report Sec. 4.0) Quantity Units Unit Price Construction to Construction to Construction General Conditions Permitting Fees 0% % \$ 10% 10%			SUMMARY				
General Conditions 10% % \$ 130; Preconstruction Services 2% % % \$ 130; Exclution 7% % % \$ 100; \$ 240; Structural Busurance 7% % % % \$ 100; \$ 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 421; 330; 33; 441; 330; 33; 441; 100;	Description	(Ref. Seismic Evaluation	Quantity	Units	Unit Price		Total Price for onstruction Item
Preconstruction Services 2% % \$ 26() Escalation 7% % % \$ 102() Sonding & Insurance 7% % % \$ 433 Contractor Profit & Overhead 6% % \$ 389,4 Sonding & Insurance General Conditions Subtotal \$ 389,4 Misc MEP N1, N2, N3, N5, N11, N12 1 Lump Sum \$ \$ 44,600.00 \$ \$ 84,4 Misc MEP N1, N2, N3, N5, N11, N12 1 Lump Sum \$ \$ 44,600.00 \$ \$ 84,4 Misc Non-Structural NM, N8, N10 1 Lump Sum \$ \$ 84,600.00 \$ \$ 84,600.00 \$ \$ 84,600.00 \$ \$ 84,600.00 \$ \$ 84,600.00 \$ \$ 84,600.00 \$ \$ 84,600.00 \$ \$ 282,6 \$ 5 253,660 \$ 1,681,100.00 \$ \$ 2			GENERAL CONDITIO	NS			
Banding A Insurance Contractor Profit & Overhead 3% 6% % \$ 4.3. 5 Contractor Profit & Overhead 6% % Ceneral Conditions Subtotal \$ 838,4 Contractor Profit & Overhead Non-Structural Elements Ceneral Conditions Subtotal \$ 338,4 Misc MEP Nd. KM EP Nd. NB, N10 1 Lump Sum \$ 84,400.00 \$ 84,40 Misc MEP Nd. NB, N10 1 Lump Sum \$ 84,600.00 \$ 84,40 Misc MEP Nd. NB, N10 1 Lump Sum \$ 84,600.00 \$ 84,40 Misc MEP N1, N2, N3, N5, N11, N12 1 Lump Sum \$ 84,600.00 \$ 84,40 Misc MEP NnStructural Subtotal \$ 118,5 118,5 118,5 118,5 222,60 Subtotal \$ 228,66 Subtotal Construction Cost \$ 1,691,100.00 \$ 238,96.00<							130,167.5 26,033.5
General Conditions Subtotal \$ 389,4 Non-Structural Elements Kin N2, N3, N5, N11, N12 1 Lump Sum \$ 84,600.00 \$ 84,4 Misc Non-Structural N1, N2, N3, N5, N11, N12 1 Lump Sum \$ 33,900.00 \$ 329,260.00 \$ 229,260.00 \$ 229,260.00 \$ 229,260.00 \$ 229,200.00 \$ 229,200.00 \$ 239,900.00 \$ 1,944,766 \$ 209,000 \$ 213,900.00 \$ 213,900.00 \$ 213,900.00 \$ 1,944,766 \$ 213,900.00 \$ 19,400.00 \$ 19,400.00 \$ 19,400.00 \$ 19,400.00 \$ 19,400.00 \$ 19,400.00 \$ 19,400.00 \$ 19,400.00 \$ 19,400.00 \$ 19,400.00 \$ 19,400.00	Bonding & Insurance		3%	%		\$	102,051.3 43,736.2 87,472.5
Misc MEP Misc Non-Structural N1, N2, N3, N5, N11, N12 N4, N8, N10 1 Lump Sum Lump Sum \$ 84,600.00 \$ 33,900.00 \$ 84,600.00 \$ 33,900.00 \$ 84,600.00 \$ 33,900.00 \$ 84,600.00 \$ 81,6		4			ral Conditions Subtotal	\$	389,461.1
Misc Non-Structural N4, N8, N10 1 Lump Sum \$ 33,900.00 \$ 32,900.00 \$ 32,900.00 \$ 32,900.00 \$ 32,900.00 \$ 32,900.00 \$ 32,900.00 \$ 32,900.00 \$ 32,900.00 <t< td=""><td></td><td>I</td><td>Non-Structural Eleme</td><td></td><td></td><td>-</td><td></td></t<>		I	Non-Structural Eleme			-	
Construction Cost Per Building Part Building Part Building Part Substal \$ 890,5 Building Part Display \$ 222,6 Sub-Total Construction Cost \$ 1,691,100 Contingency 15% \$ 253,666 Total Construction Cost \$ 1,944,766 Cost Estimate Summary \$ 29,200.00 \$ 1,944,766 Structural / Rehabilitation Engineering \$ 29,200.00 \$ 21,900.00 \$ 21,900.00 Structural / Rehabilitation Engineering \$ 21,900.00 \$ 19,400.00 \$ 19,400.00 Structural / Rehabilitation Engineering \$ 1,940.00 \$ 19,400.00 \$ 19,400.00 Seismic Feasibility Study Reimbursement \$ 1,691,100.00 \$ 1,940.00 \$ 58,30 Construction \$ 1,691,100.00 \$ 58,300.00 \$ 58,300.00 \$ 58,300.00 Permitting Fees \$ 58,300.00 \$ 58,300.00 \$ 25,4							84,600.0(33,900.0(
Building Part 'C' Subtotal \$ 890,5 Building Part 'D' Subtotal \$ 292,6 Sub-Total Construction Cost \$ 1,691,100 Contingency 15% \$ 253,665 Total Construction Cost \$ 1,944,765 Cost Estimate Summary Engineering \$ 29,200.00 \$ 29,200.00 Structural / Rehabilitation Engineering \$ 29,200.00 \$ 213,900.00 Geotechnical Consulting \$ 19,400.00 \$ 19,400.00 Materials Testing for Design \$ 19,400.00 \$ 19,400.00 Seismic Feasibility Study Reimbursement \$ 1,691,100.00 \$ 1,759,1 Construction \$ 1,691,100.00 \$ 9,700.00 \$ 9,700.00 Special Inspection Services for Construction \$ 9,700.00 \$ 9,700.00 Permitting Fees \$ 58,300.00 \$ 25,4				١	Non-Structural Subtotal	\$	118,500.0
Building Part 'D' Subtotal \$ 292,6 Building Part 'D' Subtotal Construction Cost Sub-Total Construction Cost \$ 1,691,100 Contingency 15% \$ 253,664 Contingency 15% \$ 253,664 Total Construction Cost \$ 1,944,765 Cost Estimate Summary Engineering \$ 29,200.0 \$ 29,200.0 \$ 29,200.0 \$ 29,200.0 \$ 281,9 \$ 29,200.0 \$ 281,9 \$ 29,200.0 \$ 29,200.0 \$ 29,200.0 \$ 281,9 \$ 29,200.0 \$ 281,9 \$ 29,200.0 \$ 29,200.0 \$ 281,9 \$ 29,200.0 \$ 29,200.0 \$ 281,9 \$ 29,200.0 \$ 281,9 \$ 29,200.0 \$ 281,9 \$ 29,200.0 \$ 281,9 \$ 29,200.0 \$ 281,9 \$ 29,200.0 \$ 281,9 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 281,9 \$ 29,200.00 \$ 29,200.00 \$ 281,9 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00 \$ 29,200.00		Const	ruction Cost Per Build	ling Part			
Sub-Total Construction Cost\$ 1,691,100Contingency15%\$ 253,663Total Construction Cost\$ 1,944,764Cost Estimate SummaryEngineering Architectural Consulting Structural / Rehabilitation Engineering Geotechnical Consulting Materials Testing for Design Seismic Feasibility Study Reimbursement Construction Management Construction Special Inspection Services for Construction Special Inspection Services for Construction Permitting Fees\$ 1,691,100.00 \$ 9,700.00 \$ 9,700.00\$ 1,691,100.00 \$ 9,700.00 \$ 9,700.00 \$ 58,300.00				Βι	uilding Part 'C' Subtotal	\$	890,500.0
Contingency15%\$ 253,663Total Construction Cost\$ 1,944,764Cost Estimate SummaryEngineering Architectural Consulting Structural / Rehabilitation Engineering Geotechnical Consulting Materials Testing for Design Seismic Feasibility Study Reimbursement Construction Management Construction Special Inspection Services for Construction Permitting Fees Relocation of FF&E\$ 1,691,100.00 \$ 9,700.00\$ 254				Βι	uilding Part 'D' Subtotal		292,675.0
Total Construction Cost \$ 1,944,764 Total Construction Cost \$ 1,944,764 Cost Estimate Summary Engineering \$ 29,200.0 \$ 281,9 Architectural Consulting \$ 29,200.0 \$ 29,200.0 \$ 213,900.00 \$ 19,400.00 Structural / Rehabilitation Engineering \$ 19,400.00 \$ 19,400.00 \$ 19,400.00 \$ 519,400.00 \$ 58,300.00 \$ 58,330.00 \$ 58,330.00 \$ 58,300.00 \$ 58,300.00 \$ 58,300.00 \$ 58,300.00 \$ 25,4 Sub-Total Construction of FF&E Engineering \$ 25,4 \$ 25,4 \$ 25,4							1,691,100.00
Cost Estimate Summary Engineering Architectural Consulting Structural / Rehabilitation Engineering Geotechnical Consulting \$ 29,200.0 \$ 213,900.00 \$ 19,400.00 \$ 19,400.00 \$ 19,400.00 \$ 19,400.00 \$ 19,400.00 \$ 19,400.00 \$ 1,691,100.00 Special Inspection Services for Construction Special Inspection Services for Construction Permitting Fees \$ 1,691,100.00 \$ 9,700.00 \$ 58,300.00 \$ 1,691,100.00 \$ 9,700.00 \$ 58,300.00 \$ 1,691,100.00 \$ 9,700.00 \$ 58,300.00							253,665.00
Engineering * 29,200.00 \$ 213,900.00 Structural / Rehabilitation Engineering Geotechnical Consulting \$ 213,900.00 \$ Materials Testing for Design Seismic Feasibility Study Reimbursement \$ 19,400.00 \$ Construction Management Construction Sub-Total Construction Cost Special Inspection Services for Construction Permitting Fees \$ 1,691,100.00 \$ Permitting Fees \$ 58,300.00 \$ \$					Construction Cost	\$	1,944,765.00
Architectural Consulting \$ 29,200.0 Structural / Rehabilitation Engineering \$ 213,900.00 Geotechnical Consulting \$ 19,400.00 Materials Testing for Design \$ 19,400.00 Seismic Feasibility Study Reimbursement \$ 19,400.00 Construction Management \$ 1,691,100.00 Sub-Total Construction Cost \$ 1,691,100.00 Special Inspection Services for Construction \$ 9,700.00 Permitting Fees \$ 58,300.00 Relocation of FF&E ¥ 25,4			Cost Estimate Summa	ary			
Construction Management \$ 58,3 Construction \$ 1,691,100.0 Special Inspection Services for Construction \$ 1,691,000.0 Permitting Fees \$ 58,300.0 Relocation of FF&E \$ 25,4	Architectural Consulting Structural / Rehabilitation Engineering Geotechnical Consulting Materials Testing for Design				\$ 213,900.00 \$ 19,400.00 \$ 19,400.00	\$	281,900.00
	Construction Management Construction Sub-Total Construction Cost Special Inspection Services for Construction Permitting Fees				\$ 1,691,100.00 \$ 9,700.00	\$	58,300.0 1,759,100.0
	Relocation of FF&E Contingency					\$ \$	25,400.0 253.665.0

г

		BUILDING PART -	'C'				
Description	Deficiencies (Ref. Seismic Evaluation Report Sec. 4.0)	Quantity	Units	L	Jnit Price		al Price for truction Item
	Dem	olition & Asbestos A	batement				
Soft Demolition Abatement Built-Up Roof Demo	S3, S5, S6, S7, S8, S10 S1, S6, S7, S8, S9, S10 S1, S12, S13, S14	9000 4800 8400	Square Foot Square Foot Square Foot	\$ \$ \$	5.00	\$ \$ \$	18,000.00 24,000.00 33,600.00
			Demolitio	on & Asbe	estos Subtotal	\$	75,600.00
	Foundatio	n / Floor Strengthenir	ng Construction				
Bolting of Extg Walls to footings Floor Finish Patch / Replacement Spread Footings for Columns / Holdown Micropile Micropile Caps	\$10 \$6, \$7, \$8, \$9, \$10 N9 \$5 \$3	1100 800 6 82 82 82	Linear Foot Square Foot Each Each Each	\$ \$ \$	7.00 2,500.00 4,500.00	\$ \$ \$ \$	38,500.00 5,600.00 15,000.00 369,000.00 82,000.00
			Fou	undation L	evel Subtotal	\$	510,100.00
	Wal	II Strengthening Cons	struction				
Painting of Wall Sheathing of Existing Walls Cantilever Columns Sheathing of Existing Walls Interior Wall Finish Repair Brick Veneer Ties	S6, S7, S8, S10 S6, S7, S8 N9 S6, S7, S8 S6, S7, S8, S10 N6, N7, N8	9000 9000 6 1000 9000 400	Square Foot Square Foot Each Square Foot Square Foot Square Foot	\$ \$ \$ \$	5.00 1,500.00 5.00 2.00	\$ \$ \$ \$ \$ \$ \$	27,000.00 45,000.00 9,000.00 5,000.00 18,000.00 12,000.00
			Wall	Strengthe	ening Subtotal	\$	116,000.00
		of Strengthening Con	struction				
New Roof Sheathing Diaphragm Attachments - In-Plane Shear New Single Ply Roof	S12, S13, S14 S1, S6, S7, S8 S12, S13, S14	13900 1100 13900	Square Foot Linear Foot Square Foot	\$ \$ \$	20.00	\$ \$ \$	55,600.00 22,000.00 111,200.00
			Roof	Strengthe	ening Subtotal	\$	188,800.0
			uilding Part 'C' - Total	,	ů.		890.500.00

		BUILDING PART -	'D'				
Description	Deficiencies (Ref. Seismic Evaluation Report Sec. 4.0)	Quantity	Units	U	nit Price		al Price for truction Item
	Dem	olition & Asbestos A	batement				
Soft Demolition	S3, S5, S6, S7, S8, S10	4500	Square Foot	\$		\$	9,000.0
Abatement Built-Up Roof Demo	S1, S6, S7, S8, S9, S10 S1, S12, S13, S14	1500 2700	Square Foot Square Foot	\$ \$		\$ \$	7,500.00 10,800.00
			Demolitio	on & Asbe	stos Subtotal	\$	27,300.00
	Foundatio	n / Floor Strengtheni	ng Construction				
Bolting of Extg Walls to footings	S10	300	Linear Foot	\$	35.00	\$	10,500.00
Floor Finish Patch / Replacement	S6, S7, S8, S9, S10	725	Square Foot	\$	7.00	\$	5,075.00
Spread Footings for Columns / Holdown	N9	3	Each	\$		\$	7,500.0
Micropile	S5 S3	27 27	Each Each	\$ \$		\$ \$	121,500.0
Micropile Caps		21	Each	¢	1,000.00	Þ	27,000.00
			Fou	Indation Lo	evel Subtotal	\$	171,575.00
	Wa	II Strengthening Con	struction				
Painting of Wall	S6, S7, S8, S10	4500	Square Foot	\$	3.00	\$	13,500.0
Sheathing of Existing Walls	S6, S7, S8	3000	Square Foot	\$	5.00	\$	15,000.0
Cantilever Columns	N9	3	Each	\$	1,500.00	\$	4,500.0
New 2x Framed Shear Walls	S6, S7, S8	500	Square Foot	\$	10.00	\$	5,000.0
Interior Wall Finish Repair	S6, S7, S8, S10	3000	Square Foot	\$	2.00	\$	6,000.0
Brick Veneer Ties	N6, N7, N8	160	Square Foot	\$	30.00	\$	4,800.00
			Wall	Strengthe	ning Subtotal	\$	48,800.00
	Roc	of Strengthening Con	struction				
New Roof Sheathing	S12, S13, S14	3250	Square Foot	\$	4.00	\$	13,000.00
Diaphragm Attachments - In-Plane Shear	S1, S6, S7, S8	300	Linear Foot	\$		\$	6,000.0
New Single Ply Roof	S12, S13, S14	3250	Square Foot	\$	8.00	\$	26,000.0
	l		Roof	Strengther	ning Subtotal	¢	45.000.0
		-	Building Part 'D' - Total	•	J.		292.675.00



Appendix D: Benefit Cost Analysis Worksheets

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Oregon Seismic Rehabilitation Grant Application: Benefit-Cost Analysis

Entity:	Lane Education Service District			
Point of Contact	Bradley Johnston			
Telephone:	(541)461-8260			
E-Mail:	bjohnston@lesd.k12.or.us			
BCA File Name:	BCA-WestmorelandWest		BCA Date:	12/21/2019
Building Name:	Lane School Westmoreland Can	pus Phase 1		
Site ID:	Westmoreland_ES			
Facility Use:	School			

Is the Building in the Oregon BCA Tool Database: Yes or No?

How Many Structurally Different Building Parts Are There?

Unique Building ID Number	Building Part Square Footage	Percent of Total SF	Percent of Occupancy	Percent of Operating Budget	Building Part Being Retrofitted?
Westmoreland_ESA	25,300	43.98%	43.98%	43.98%	No
Westmoreland_ESB	3,800	6.61%	6.61%	6.61%	No
Westmoreland_ESC	14,930	25.96%	25.96%	25.96%	Yes
Westmoreland_ESD	2,620	4.55%	4.55%	4.55%	Yes
Westmoreland_ESE	2,950	5.13%	5.13%	5.13%	No
Westmoreland_ESF	5,800	10.08%	10.08%	10.08%	No
Westmoreland_ESG	2,120	3.69%	3.69%	3.69%	No
Totals:	57,520	100.00%	100.00%	100.00%	

Seismic Retrofit Cost Estimate per SRGP Application:

\$2,378,365

No

Database

Not Listed

User-Defined

7

Page 1

Benefit-Cost Analysis: Summary Results Lane School Westmoreland Campus Phase 1

Building Part	Benefits	Benefits by Cat	egory
Westmoreland_ESA		Avoided Damages a	nd Losses
Westmoreland_ESB		Building Damage	\$273,857
Westmoreland_ESC	\$608,699	Contents Damage	\$68,464
Westmoreland_ESD	\$106,818	Displacement Costs	\$36,600
Westmoreland_ESE		Loss of Function Costs	\$9,849
Westmoreland_ESF		Casualties	\$326,747
Westmoreland_ESG		Total	\$715,517
Total Benefits	\$715,517		
Total Cost	\$2,378,365		
Benefit-Cost	0.301		
Ratio	0.301		

Occupancy Data

For benefit-cost analysis, the average occupancy on a 24/7/365 basis is used for casualty calculations.

Enter data below ONLY for the occupancy categories applicable to this building - all other green cell entries should be left blank. There are entries below for: employees, visitors, students, meetings or special events and patients.

NOTE: for buildings with similar occupancies each month, complete the tables on the left side only.

NOTE: For buildings with different summer occupancies, complete the tables both on the left and right sides. If this does not apply, enter "0" for number of summer months

Number of

Employees: 12 Months per Year or Academic Year for Schools						
Day of Week	Time of Day	Hours per Day	Average Employees in Building	Calculated 24/7/365 Occupancy		
Monday - Friday	Day	8	55	9.795		
Monday - Friday	Evening	8	5	0.890		
Monday - Friday	Night					
Saturday	Day					
Saturday	Evening					
Saturday	Night					
Sunday	Day					
Sunday	Evening					
Sunday	Night					
			Subtotal:	10.685		

Employees: Summer Months		Number of Months:	3	
Day of Week	Time of Day	Hours per Day	Average Employees in Building	Calculated 24/7/365 Occupancy
Monday - Friday	Day	8	2	0.119
Monday - Friday	Evening			
Monday - Friday	Night			
Saturday	Day			
Saturday	Evening			
Saturday	Night			
Sunday	Day			
Sunday	Evening			
Sunday	Night			
			Subtotal:	0.119

Visitors: 12 Months per Year or Academic Year for Schools			
Day of Week	Average Number of Visitors Per Day	Average Time in Building (Minutes)	Calculated 24/7/365 Occupancy
Monday - Friday	5	30	0.056
Saturday			
Sunday			
		Subtotal:	0.056

Visitors: Summer Months		Number of Months:	3
Day of Week	Average Number of Visitors Per Day	Average Time in Building (Minutes)	Calculated 24/7/365 Occupancy
Monday - Friday			
Saturday			
Sunday			
		Subtotal:	

K-12 Students: Academic Year	
Average Daily Number of Students:	128
Hours per Day:	6
Days per Year:	170
Calculated 24/7/365 Occupancy:	14.904

eenege etademter	Academic	Year		
Num	ber of Wee	eks per Year	of Classes:	
Course	Class Duration (hours)	Number of Class Periods per Week	Average Number of Students per Class	Calculated 24/7/365 Occupancy
1 Hr. Courses	1			
1.5 Hr. Courses	1.5			
2 Hr. Courses	2			
3 Hr. Courses	3			
Other	N/A			
Other	N/A			
			Subtotal:	

K-12 Students: Summer School	
Average Daily Number of Students:	
Hours per Day:	
Days per Year:	
Calculated 24/7/365 Occupancy:	

College Students:	Summer S	chool		
Num	ber of Wee	ks per Year	of Classes:	
Course	Class Duration (hours)	Number of Class Periods per Week	Average Number of Students per Class	Calculated 24/7/365 Occupancy
-				
1 Hr. Courses	1			
1.5 Hr. Courses	1.5			
2 Hr. Courses	2			
3 Hr. Courses	3			
Other	N/A			
Other	N/A			
			Subtotal:	

Occupancy Data

Meetings, Sports E	vents etc			
Event	Events per Year	People per Event	Event (hours)	Calculated 24/7/365 Occupancy
IEP Meetings	130	6	1.5	0.134
Family Nights	2	50	2	0.023
Board Meeting	1	25	2	0.006
J				
			Subtotal:	0.162
			Subtoldi:	0.102

Patients				
	Total Nur	nber of In-Pa	atient Beds:	
A	/erage Dail	y Number of	f In-Patients	
	Average	Percentage	Occupancy	
Day of Week	•	Number of nts per Day	Average Time in Building (Hours)	Calculated 24/7/365 Occupancy
Monday - Friday				
Saturday				
Sunday				
		0	ut-Patients:	
			In-Patients:	
		Tot	tal Patients:	

SUMMARY OCCUPANCY DATA: Average 24/7/365 Occupancy

Occupancy Category	12 Months or Academic Year	Summer
Employees	10.685	0.119
Visitors	0.056	
Students: K-12	14.904	
Students: College		
Meetings & Special Events	0.162	N/A
Patients		N/A
Subtotals:	25.807	0.119
Avg 24/7/365 Occupancy:	25.926	

DATA DOCUMENTATION: OCCUPANCY			
	Provide brief documentation below and/or references to other documents included with your application (with page number), for the sources of the occupancy data and estimates.		
Employees: Numbers			
Employees: Hours Per Day			
Visitors: Number Per Day			
Visitors: Average Time in Building			
K-12 Students: Number			
K-12 Students: Hours Per Day			
K-12 Students: Days Per Year			
Additional Comments Re: above Occupancy Data			
College Student Occupancy Data			

	Meetings, Sports Events and Other Special Events	
NOTES:	It is <u>NOT</u> necessary to provide separate documentation for every special event listed. Rather, provide an Overview Statement of the sources of special event occupancy estimates.	
NOTES.	Provide specific documentation for high occupancy events or very frequent events with high Calculated 24/7/365 Occupancy, especially for occupancies that appear "unusual" or potentially "out of bounds."	
Overview Statement Re: Sources of Special Events Occupancy Estimates		

	Hospital Patient Data						
Number of Patient Beds							
Average Daily Number of In-Patients							
Average Daily Number of Out-Patients							
Average Time in Building for Out-Patients							

				Col	lege Student	Occupancy Data	a				Instructions			Occupancy data entered on this page are generally However, if you enter data on the Main Page for only																
These tables calc	culate	the inpu	ats requir	ed to determin	e the average 2	24/7/365 occupancy	for the class	ses in the b	uilding. The ta	ibles are	Enter requested ocurse data into the green shaded cells. Tables for the Academic Year are in Row 9, Tables for Summer School are in Row 64. Use the Other / Additional Courses tables for class durations that aren't			available for and entered for the entire school or parts of a facility, then the occupancy data on this page					See: USER GU for furth											
						bles provided to cap		int course le	ngths.		Academic Year Use the Other /	are in Row S Additional C	Tables for Su surses tables f	Immer School a or class duratio	re in Row 64. ns that aren't	a Main Page.														
Do not duplicate	i intern			ready been pr	ovided on the C	occupancy worksne	at.				specified elsew	iere or if add	itional space is	al space is required.																
	Acad	lemic Ye	er: 1 Hou Number of	Average	Student		Academic Y Class	Number of	Average	Student		Academi Class	Year: 2 Hou Number of	Average	Student		Academic Class	Year: 3 Hour Number of	Average	Student	Acadi	Class	Number of	Average	s Student	Acade	Class	Other / Addi Number of	Average	Student
Course Name	Du	mine	Class Periods	Number of Students	Hours per Week	Course Name	Duration (hours)	Class Periods	Number of Students	Hours per Week	Course Nan	e Duratio	en Periods	Number of Students	Hours per Week	Course Name	Duration (hours)	Class Periods	Number of Students	Hours per Week	Course Name	Duration (hours)	Class Periods	Number of Students	Hours per Week	Course Name	Duration (hours)	Class Periods	Average Number of Students	Hours per Week
	È	1	per Week	per Class	0.0		1.5	per Week	per Class	0.0		2	per Week	per Class	0.0		3	per Week	per Class	0.0			per Week	per Class	0.0			per Week	per Class	0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1 1			0.0		1.5 1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3 3			0.0					0.0					0.0
		1					1.5			0.0		2 2 2 2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0 0.0 0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0 0.0 0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5 1.5			0.0		2 2 2 2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2 2 2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2 2 2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5 1.5 1.5			0.0		2			0.0		3			0.0					0.0 0.0 0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5 1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1 otals:	0	0.00	0.0	-	1.5 Totals:	•	0.00	0.0		2 Total	s: 0	0.00	0.0		3 Totals:	0	0.00	0.0		Totals	0	0.00	0.0		Totals:	0	0.00	0.0
		lass N	vumber of Class	Average Number of	Student		Class	Number of Class	Average Number of	Student		Summer		Average Number of	Student		Class	Number of Class	Average Number of	Student	Summ	Class	Other / Add Number of Class	Average Number of	Student	Summe	r School: Class	Other / Add Number of Class	Average Number of	s Student
Course Name	Du (h	ration ours)	Periods per Week	Students per Class	Hours per Week	Course Name	Duration (hours)	Periods per Week	Students per Class	Hours per Week	Course Nan	e Duratio (hours		Students per Class	Hours per Week	Course Name	Duration (hours)	Periods per Week	Students per Class	Hours per Week	Course Name	Duration (hours)	Periods per Week	Students per Class	Hours per Week	Course Name	Duration (hours)	Periods per Week	Students per Class	Hours per Week
		1	per week	perclass	0.0		1.5	per week	percuss	0.0		2	per week	per class	0.0		3	per week	per class	0.0			per week	perclass	0.0			per week	perclass	0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0 0.0 0.0		3			0.0					0.0 0.0 0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3 3 0			0.0					0.0					0.0
		1			0.0		1.5 1.5 1.5			0.0		2 2 2 2			0.0		3 3 3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2 2 2			0.0		3			0.0					0.0					0.0
		1			0.0 0.0 0.0 0.0		1.5			0.0		2 2 2			0.0		3			0.0					0.0 0.0 0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0		1			0.0					0.0
		1					15			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5 1.5 1.5			0.0		2			0.0		3			0.0					0.0 0.0 0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0		1			0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5			0.0		2			0.0		3			0.0					0.0					0.0
		1			0.0		1.5 1.5 1.5			0.0		2			0.0		3			0.0 0.0 0.0					0.0					0.0
		1 1			0.0 0.0 0.0		1.5 1.5 1.5			0.0		2			0.0 0.0 0.0		3			0.0					0.0 0.0 0.0 0.0					0.0
	T	1					1.5			0.0		2			0.0		3			0.0										0.0
	1 7	1 Totals:			0.0		1.5 Totals:		_	0.0		2			0.0		3 Totals			0.0					0.0					0.0

and Campus Phase 1, Sheet: College Student Occupancy

Annual Operating Budget for this Facility

Em	ployees:				
	Classification	Number of FTEs ¹	Average Annual Salary per Employee	Total Benefits as Percent of Salary	Annual Salary and Benefits
1	Custodian	0.81	\$46,571	95.00%	\$73,559
2	Custodian	0.5	\$46,571	86.00%	\$43,311
3	Facilities Manager	0.25	\$86,632	62.00%	\$35,086
4	Teacher	10	\$54,300	70.00%	\$923,100
5	Behavior Consultant	2.9	\$71,800	63.00%	\$339,399
6	Instructional Assistant	28.88	\$21,800	103.00%	\$1,278,056
7	Program Assistant	1	\$39,500	81.00%	\$71,495
8	Special Ed Supervisor	0.93	\$86,000	60.00%	\$127,968
9					\$0
10					\$0
	Total Number of FTEs:	45.27		Subtotal:	\$2,891,973

¹ FTEs: Full time equivalents

Other Building Expenses

Category		Annual Cost
Supplies	\$58,000	
Building Maintenance		\$54,000
Utilities		\$56,000
Insurance		\$16,000
Rent		\$0
Average Annual Capital Goods		\$53,000
OTHER: specify below		
	-	
Percent of District Office/Headquarters Annual Operating Budget Attributed to This Building:	6.70%	\$76,195
If rent is zero (building owned), a proxy rent is cal automatically, based on the value of the building:	\$1,449,504	
	Subtotal:	\$1,762,699

Total Building Annual Operating Budget: \$4,654,672

Annual Operating Budget for this Facility

For entities with multiple facilities, a fraction of the operating budget for a District Office of Headquarters building may be attributed to the building being retrofitted. That is, the annual operating budget for the building above may include part of the operating budget for the District Office or Headquarters Building. If so, complete the following tables:

Dis	trict Office/Headquarters Building Empl	oyees			
	Classification	Number of FTEs ¹	Average Annual Salary per Employee	Total Benefits as Percent of Salary	Annual Salary and Benefits
1	Custodian	0.5	\$46,571	86.00%	\$43,311
2	Custodian	0.5	\$35,776	80.00%	\$32,198
3	Custodian	0.19	\$46,571	95.00%	\$17,255
4	Executive Assistant	0.2	\$66,669	75.00%	\$23,334
5	Facilities Manager	0.75	\$86,632	62.00%	\$105,258
6					\$0
7					\$0
8					\$0
9					\$0
10					\$0
	Total Number of FTEs:	2.14		Subtotal:	\$221,356

District Office/Headquarters Building Expenses

Category		Annual Cost
Supplies		\$31,000
Building maintenance		\$59,000
Utilities		\$71,000
Insurance		\$19,000
Rent		\$0
Average Annual Capital Goods		\$151,000
OTHER: specify below		
Enter replacement value of building:	\$8,355,452	
If rent is zero (building owned), a proxy rent is ca	Iculated	\$584,882
	Subtotal:	\$915,882

Total Annual Operating Budget for District Office/Headquarters Building: \$1,137,238

Lane School Westmoreland Campus Phase 1, Sheet: Budget

DOCUMENTATION: ANNUAL OPERATING BUDGET							
NOTE:	The Annual Operating Budget is used as a "proxy" for the value of services provided from a building and is used to count the benefits of avoiding loss of service in future earthquake events.						
Operating Budget by Categories							
Percent of District Office or Headquarters Annual Operating Budget Attributed to the Facility							

Building Part A: Data for Benefit-Cost Analysis

Building Name:	Lane School Westmoreland Campus Phase 1
Building ID:	Westmoreland_ESA
Building Part Name / Description:	Classroom Wing (Not Included in Scope)

Evaluation for Building Part A

Seismic Hazard Data	Seismic Hazard Data					
Region of Seismicity	Moderately High					
PGA Ground Motion (g)	2% in 50 year	0.400				
	5% in 50 year	0.287				
	10% in 50 year	0.189				
	20% in 50 year	0.083				
Spectral Accelerations (g)	S _{xs} , 2% in 50 year	0.903				
	S _{x1} , 2% in 50 year	0.613				
	S _{xs} , 10% in 50 year	0.408				
	S _{x1} , 10% in 50 year	0.265				

Data Entry Item	User Entered Values	Default Values	Used for BCA
Site Data			
County	Lane		Lane
Decimal Latitude	44.041		44.041
Decimal Longitude	123.129		123.129
Soil Type	D		D
Construction Data			
Primary Structure Type (FEMA 154)	W2		W2
Number of Stories	1		1
Year Built	1950		1950
Rapid Visual Screening Data			
Severe Vertical Irregularity	No		No
Moderate Vertical Irregularity	Yes		Yes
Plan Irregularity	Yes		Yes
Pre-Code	Yes		Yes
Post-Benchmark	No		No
Building Data			
Historic Importance	None	None	None
Historic Adjustment Modifier	N/A	N/A	1.00
Building Square Footage - SF	25.300	N/A	25,300
Building Replacement - \$/SF		\$360.00	\$360.00
Building Replacement Value - \$	N/A	N/A	\$9,108,000
Historic Building Replacement - \$/SF	N/A	N/A	\$360.00
Historic Building Replacement Value - \$	N/A	N/A	\$9,108,000
Contents Value - % of Building Value		25%	25%
Displacement Costs - \$/SF/month		\$2.50	\$2.50
Displacement Costs - One Time		\$3.00	\$3.00
Average Annual Occupancy	11.40	11.40	11.40
Annual Operating Budget	\$2,047,344	\$2,047,344	\$2,047,344
Seismic Fragility Curves			
Before Mitigation			
Slight Damage State		0.10	0.10
Moderate Damage State		0.16	0.16
Extensive Damage State		0.31	0.31
Complete Damage State		0.50	0.50
Beta		0.66	0.66
After Mitigation	· · · ·		
Retrofit Building Type		W2	W2
Retrofit Performance Objective		LS	LS
Slight Damage State		0.10	0.10
Moderate Damage State		0.16	0.16
Extensive Damage State		0.31	0.31
Complete Damage State		0.50	0.50
Beta		0.66	0.66

	Data Documentation: Building Part A						
	ntation below and/or references to other documents included with your application ut <u>ONLY for data entries in Column C</u> , which replace the default values in Column D.						
Soil Type							
Primary Structure Type							
Number of Stories							
Year Built							
Severe Vertical Irregularity							
Moderate Vertical Irregularity							
Plan Irregularity							
Pre-Code							
Post-Benchmark							
Historic Importance (if not none)							
Building Square Footage Building Replacement Value \$/SF							
Contents Value % of Building Value							
Displacement Costs One Time							
Displacement Costs \$/SF/month							
Fragility Curve Parameters Before Mitigation							
Fragility Curve Parameters After Mitigation							
Other Comments							

Building Part B: Data for Benefit-Cost Analysis

Building Name:	Lane School Westmoreland Campus Phase 1
Building ID:	Westmoreland_ESB
Building Part Name / Description:	Gymnasium (Not Included in Scope)

Evaluation for Building Part B

Seismic Hazard Data		
Region of Seismicity	Moderately High	
PGA Ground Motion (g)	2% in 50 year	0.400
	5% in 50 year	0.287
	10% in 50 year	0.189
	20% in 50 year	0.083
Spectral Accelerations (g)	S _{xs} , 2% in 50 year	0.903
	S _{x1} , 2% in 50 year	0.613
	S _{xs} , 10% in 50 year	0.408
	S _{x1} , 10% in 50 year	0.265

Data Entry Item	User Entered Values	Default Values	Used for BCA
Site Data			
County	Lane		Lane
Decimal Latitude	44.041		44.041
Decimal Longitude	123.129		123.129
Soil Type	D		D
Construction Data			
Primary Structure Type (FEMA 154)	W2		W2
Number of Stories	1		1
Year Built	1950		1950
Rapid Visual Screening Data			
Severe Vertical Irregularity	No		No
Moderate Vertical Irregularity	No		No
Plan Irregularity	Yes		Yes
Pre-Code	Yes		Yes
Post-Benchmark	No		No
Building Data			
Historic Importance	None	None	None
Historic Adjustment Modifier	N/A	N/A	1.00
Building Square Footage - SF	3,800	N/A	3.800
Building Replacement - \$/SF	\$360.00	\$360.00	\$360.00
Building Replacement Value - \$	N/A	N/A	\$1,368,000
Historic Building Replacement - \$/SF	N/A	N/A	\$360.00
Historic Building Replacement Value - \$	N/A	N/A	\$1,368,000
Contents Value - % of Building Value	25%	25%	25%
Displacement Costs - \$/SF/month	\$2.50	\$2.50	\$2.50
Displacement Costs - One Time	\$3.00	\$3.00	\$3.00
Average Annual Occupancy	1.71	1.71	1.71
Annual Operating Budget	\$307,506	\$307,506	\$307,506
Seismic Fragility Curves			
Before Mitigation			
Slight Damage State		0.11	0.11
Moderate Damage State		0.17	0.17
Extensive Damage State		0.33	0.33
Complete Damage State		0.54	0.54
Beta		0.66	0.66
After Mitigation			
Retrofit Building Type	W2	W2	W2
Retrofit Performance Objective	IO	LS	10
Slight Damage State		0.11	0.11
Moderate Damage State		0.17	0.17
Extensive Damage State		0.33	0.33
Complete Damage State		0.54	0.54
Beta		0.66	0.66

Data Documentation: Building Part B		
	ntation below and/or references to other documents included with your application ut <u>ONLY for data entries in Column C</u> , which replace the default values in Column D.	
Soil Type		
Primary Structure Type		
Number of Stories		
Year Built		
Severe Vertical Irregularity		
Moderate Vertical Irregularity		
Plan Irregularity		
Pre-Code		
Post-Benchmark		
Historic Importance (if not none)		
Building Square Footage		
Building Replacement Value \$/SF		
Contents Value % of Building Value		
Displacement Costs One Time		
Displacement Costs \$/SF/month		
Fragility Curve Parameters Before Mitigation		
Fragility Curve Parameters After Mitigation		
Other Comments		

Building Part C: Data for Benefit-Cost Analysis

Building Name:	Lane School Westmoreland Campus Phase 1
Building ID:	Westmoreland_ESC
Building Part Name / Description:	Classroom Wing - Limited Safety

Evaluation for Building Part C

Seismic Hazard Data		
Region of Seismicity	Moderately High	
PGA Ground Motion (g)	2% in 50 year	0.400
	5% in 50 year	0.287
	10% in 50 year	0.189
	20% in 50 year	0.083
Spectral Accelerations (g)	S _{xs} , 2% in 50 year	0.903
	S _{x1} , 2% in 50 year	0.613
	S _{xs} , 10% in 50 year	0.408
	S _{x1} , 10% in 50 year	0.265

Data Entry Item	User Entered Values	Default Values	Used for BCA
Site Data			
County	Lane		Lane
Decimal Latitude	44.041		44.041
Decimal Longitude	123.129		123.129
Soil Type	D		D
Construction Data			
Primary Structure Type (FEMA 154)	W2		W2
Number of Stories	1		1
Year Built	1950		1950
Rapid Visual Screening Data			
Severe Vertical Irregularity	No		No
Moderate Vertical Irregularity	Yes		Yes
Plan Irregularity	Yes		Yes
Pre-Code	Yes		Yes
Post-Benchmark	No		No
Building Data			
Historic Importance	None	None	None
Historic Adjustment Modifier	N/A	N/A	1.00
Building Square Footage - SF	14,930	N/A	14,930
Building Replacement - \$/SF		\$360.00	\$360.00
Building Replacement Value - \$	N/A	N/A	\$5,374,800
Historic Building Replacement - \$/SF	N/A	N/A	\$360.00
Historic Building Replacement Value - \$	N/A	N/A	\$5,374,800
Contents Value - % of Building Value		25%	25%
Displacement Costs - \$/SF/month		\$2.50	\$2.50
Displacement Costs - One Time		\$3.00	\$3.00
Average Annual Occupancy	6.73	6.73	6.73
Annual Operating Budget	\$1,208,175	\$1,208,175	\$1,208,175
Seismic Fragility Curves			
Before Mitigation			
Slight Damage State		0.10	0.10
Moderate Damage State		0.16	0.16
Extensive Damage State		0.31	0.31
Complete Damage State		0.50	0.50
Beta		0.66	0.66
After Mitigation			
Retrofit Building Type	W2	W2	W2
Retrofit Performance Objective	LS	LS	LS
Slight Damage State		0.22	0.22
Moderate Damage State		0.43	0.43
Extensive Damage State		0.85	0.85
Complete Damage State		1.52	1.52
Beta		0.62	0.62

Data Documentation: Building Part C		
	ntation below and/or references to other documents included with your application ut <u>ONLY for data entries in Column C</u> , which replace the default values in Column D.	
Soil Type		
Primary Structure Type		
Number of Stories		
Year Built		
Severe Vertical Irregularity		
Moderate Vertical Irregularity		
Plan Irregularity		
Pre-Code		
Post-Benchmark		
Historic Importance (if not none)		
Building Square Footage		
Building Replacement Value \$/SF		
Contents Value % of Building Value		
Displacement Costs One Time		
Displacement Costs \$/SF/month		
Fragility Curve Parameters Before Mitigation		
Fragility Curve Parameters After Mitigation		
Other Comments		

Building Part D: Data for Benefit-Cost Analysis

Building Name:	Lane School Westmoreland Campus Phase 1
Building ID:	Westmoreland_ESD
Building Part Name / Description:	Classroom Wing - Limited Safety

Evaluation for Building Part D

Seismic Hazard Data		
Region of Seismicity	Moderately High	
PGA Ground Motion (g)	2% in 50 year	0.400
	5% in 50 year	0.287
	10% in 50 year	0.189
	20% in 50 year	0.083
Spectral Accelerations (g)	S _{xs} , 2% in 50 year	0.903
	S _{x1} , 2% in 50 year	0.613
	S _{xs} , 10% in 50 year	0.408
	S _{x1} , 10% in 50 year	0.265

Data Entry Item	User Entered Values	Default Values	Used for BCA
Site Data			
County	Lane		Lane
Decimal Latitude	44.041		44.041
Decimal Longitude	123.129		123.129
Soil Type	D		D
Construction Data			
Primary Structure Type (FEMA 154)	W2		W2
Number of Stories	1		1
Year Built	1950		1950
Rapid Visual Screening Data			
Severe Vertical Irregularity	No		No
Moderate Vertical Irregularity	Yes		Yes
Plan Irregularity	Yes		Yes
Pre-Code	Yes		Yes
Post-Benchmark	No		No
Building Data			
Historic Importance	None	None	None
Historic Adjustment Modifier	N/A	N/A	1.00
Building Square Footage - SF	2,620	N/A	2,620
Building Replacement - \$/SF	_,	\$360.00	\$360.00
Building Replacement Value - \$	N/A	N/A	\$943,200
Historic Building Replacement - \$/SF	N/A	N/A	\$360.00
Historic Building Replacement Value - \$	N/A	N/A	\$943,200
Contents Value - % of Building Value		25%	25%
Displacement Costs - \$/SF/month		\$2.50	\$2.50
Displacement Costs - One Time		\$3.00	\$3.00
Average Annual Occupancy	1.18	1.18	1.18
Annual Operating Budget	\$212,017	\$212,017	\$212,017
Seismic Fragility Curves		·	
Before Mitigation			
Slight Damage State		0.10	0.10
Moderate Damage State		0.16	0.16
Extensive Damage State		0.31	0.31
Complete Damage State		0.50	0.50
Beta		0.66	0.66
After Mitigation			
Retrofit Building Type	W2	W2	W2
Retrofit Performance Objective	LS	LS	LS
Slight Damage State		0.22	0.22
Moderate Damage State		0.43	0.43
Extensive Damage State		0.85	0.85
Complete Damage State		1.52	1.52
Beta		0.62	0.62

Data Documentation: Building Part D		
	ntation below and/or references to other documents included with your application ut <u>ONLY for data entries in Column C</u> , which replace the default values in Column D.	
Soil Type		
Primary Structure Type		
Number of Stories		
Year Built		
Severe Vertical Irregularity		
Moderate Vertical Irregularity		
Plan Irregularity		
Pre-Code		
Post-Benchmark		
Historic Importance (if not none)		
Building Square Footage		
Building Replacement Value \$/SF		
Contents Value % of Building Value		
Displacement Costs One Time		
Displacement Costs \$/SF/month		
Fragility Curve Parameters Before Mitigation		
Fragility Curve Parameters After Mitigation		
Other Comments		

Building Part E: Data for Benefit-Cost Analysis

Building Name:	Lane School Westmoreland Campus Phase 1
Building ID:	Westmoreland_ESE
Building Part Name / Description:	Cafeteria (Not Included in Scope)

Evaluation for Building Part E

Seismic Hazard Data		
Region of Seismicity	Moderately High	
PGA Ground Motion (g)	2% in 50 year	0.400
	5% in 50 year	0.287
	10% in 50 year	0.189
	20% in 50 year	0.083
Spectral Accelerations (g)	S _{xs} , 2% in 50 year	0.903
	S _{x1} , 2% in 50 year	0.613
	S _{xs} , 10% in 50 year	0.408
	S _{x1} , 10% in 50 year	0.265

Data Entry Item	User Entered Values	Default Values	Used for BCA
Site Data			
County	Lane		Lane
Decimal Latitude	44.041		44.041
Decimal Longitude	123.129		123.129
Soil Type	D		D
Construction Data			
Primary Structure Type (FEMA 154)	W2		W2
Number of Stories	1		1
Year Built	1950		1950
Rapid Visual Screening Data			
Severe Vertical Irregularity	No		No
Moderate Vertical Irregularity	Yes		Yes
Plan Irregularity	No		No
Pre-Code	Yes		Yes
Post-Benchmark	No		No
Building Data			
Historic Importance	None	None	None
Historic Adjustment Modifier	N/A	N/A	1.00
Building Square Footage - SF	2,950	N/A	2,950
Building Replacement - \$/SF		\$360.00	\$360.00
Building Replacement Value - \$	N/A	N/A	\$1,062,000
Historic Building Replacement - \$/SF	N/A	N/A	\$360.00
Historic Building Replacement Value - \$	N/A	N/A	\$1,062,000
Contents Value - % of Building Value		25%	25%
Displacement Costs - \$/SF/month		\$2.50	\$2.50
Displacement Costs - One Time		\$3.00	\$3.00
Average Annual Occupancy	1.33	1.33	1.33
Annual Operating Budget	\$238,722	\$238,722	\$238,722
Seismic Fragility Curves			
Before Mitigation			
Slight Damage State		0.11	0.11
Moderate Damage State		0.18	0.18
Extensive Damage State		0.34	0.34
Complete Damage State		0.56	0.56
Beta		0.66	0.66
After Mitigation			
Retrofit Building Type	W2	W2	W2
Retrofit Performance Objective	IO	LS	IO
Slight Damage State		0.11	0.11
Moderate Damage State		0.18	0.18
Extensive Damage State		0.34	0.34
Complete Damage State		0.56	0.56
Beta		0.66	0.66

Data Documentation: Building Part E		
	ntation below and/or references to other documents included with your application ut <u>ONLY for data entries in Column C</u> , which replace the default values in Column D.	
Soil Type		
Primary Structure Type		
Number of Stories		
Year Built		
Severe Vertical Irregularity Moderate Vertical Irregularity		
Plan Irregularity		
Pre-Code		
Post-Benchmark		
Historic Importance (if not none)		
Building Square Footage		
Building Replacement Value \$/SF		
Contents Value % of Building Value		
Displacement Costs One Time		
Displacement Costs \$/SF/month		
Fragility Curve Parameters Before Mitigation		
Fragility Curve Parameters After Mitigation		
Other Comments		

Building Part F: Data for Benefit-Cost Analysis

Building Name:	Lane School Westmoreland Campus Phase 1
Building ID:	Westmoreland_ESF
Building Part Name / Description:	Classroom Wing (Not Included in Scope)

Evaluation for Building Part F

Seismic Hazard Data		
Region of Seismicity	Moderately High	
PGA Ground Motion (g)	2% in 50 year	0.400
	5% in 50 year	0.287
	10% in 50 year	0.189
	20% in 50 year	0.083
Spectral Accelerations (g)	S _{xs} , 2% in 50 year	0.903
	S _{x1} , 2% in 50 year	0.613
	S _{xs} , 10% in 50 year	0.408
	S _{x1} , 10% in 50 year	0.265

Data Entry Item	User Entered Values	Default Values	Used for BCA
Site Data			
County	Lane		Lane
Decimal Latitude	44.041		44.041
Decimal Longitude	123.129		123.129
Soil Type	D		D
Construction Data			
Primary Structure Type (FEMA 154)	W2		W2
Number of Stories	1		1
Year Built	1950		1950
Rapid Visual Screening Data			
Severe Vertical Irregularity	No		No
Moderate Vertical Irregularity	Yes		Yes
Plan Irregularity	Yes		Yes
Pre-Code	Yes		Yes
Post-Benchmark	No		No
Building Data			
Historic Importance	None	None	None
Historic Adjustment Modifier	N/A	N/A	1.00
Building Square Footage - SF	5,800	N/A	5,800
Building Replacement - \$/SF		\$360.00	\$360.00
Building Replacement Value - \$	N/A	N/A	\$2,088,000
Historic Building Replacement - \$/SF	N/A	N/A	\$360.00
Historic Building Replacement Value - \$	N/A	N/A	\$2,088,000
Contents Value - % of Building Value		25%	25%
Displacement Costs - \$/SF/month		\$2.50	\$2.50
Displacement Costs - One Time		\$3.00	\$3.00
Average Annual Occupancy	2.61	2.61	2.61
Annual Operating Budget	\$469,351	\$469,351	\$469,351
Seismic Fragility Curves			
Before Mitigation			
Slight Damage State		0.10	0.10
Moderate Damage State		0.16	0.16
Extensive Damage State		0.31	0.31
Complete Damage State		0.50	0.50
Beta		0.66	0.66
After Mitigation			
Retrofit Building Type		W2	W2
Retrofit Performance Objective		LS	LS
Slight Damage State		0.10	0.10
Moderate Damage State		0.16	0.16
Extensive Damage State		0.31	0.31
Complete Damage State		0.50	0.50
Beta		0.66	0.66

Data Documentation: Building Part F			
	Provide brief documentation below and/or references to other documents included with your application (with page number), but <u>ONLY for data entries in Column C</u> , which replace the default values in Column D.		
Soil Type			
Primary Structure Type			
Number of Stories			
Year Built			
Severe Vertical Irregularity			
Moderate Vertical Irregularity			
Plan Irregularity			
Pre-Code			
Post-Benchmark			
Historic Importance (if not none)			
Building Square Footage			
Building Replacement Value \$/SF			
Contents Value % of Building Value			
Displacement Costs One Time			
Displacement Costs \$/SF/month			
Fragility Curve Parameters Before Mitigation			
Fragility Curve Parameters After Mitigation			
Other Comments			

Building Part G: Data for Benefit-Cost Analysis

Building Name:	Lane School Westmoreland Campus Phase 1
Building ID:	Westmoreland_ESG
Building Part Name / Description:	Boiler Room (Not Included in Scope)

Evaluation for Building Part G

Seismic Hazard Data		
Region of Seismicity	Moderately High	
PGA Ground Motion (g)	2% in 50 year	0.400
	5% in 50 year	0.287
	10% in 50 year	0.189
	20% in 50 year	0.083
Spectral Accelerations (g)	S _{xs} , 2% in 50 year	0.903
	S _{x1} , 2% in 50 year	0.613
	S _{xs} , 10% in 50 year	0.408
	S _{x1} , 10% in 50 year	0.265

Data Entry Item	User Entered Values	Default Values	Used for BCA
Site Data			
County	Lane		Lane
Decimal Latitude	44.041		44.041
Decimal Longitude	123.129		123.129
Soil Type	D		D
Construction Data			
Primary Structure Type (FEMA 154)	URM		URM
Number of Stories	1		1
Year Built	1950		1950
Rapid Visual Screening Data			
Severe Vertical Irregularity	No		No
Moderate Vertical Irregularity	Yes		Yes
Plan Irregularity	No		No
Pre-Code	Yes		Yes
Post-Benchmark	No		No
Building Data			
Historic Importance	None	None	None
Historic Adjustment Modifier	N/A	N/A	1.00
Building Square Footage - SF	2,120	N/A	2,120
Building Replacement - \$/SF		\$360.00	\$360.00
Building Replacement Value - \$	N/A	N/A	\$763,200
Historic Building Replacement - \$/SF	N/A	N/A	\$360.00
Historic Building Replacement Value - \$	N/A	N/A	\$763,200
Contents Value - % of Building Value		25%	25%
Displacement Costs - \$/SF/month		\$2.50	\$2.50
Displacement Costs - One Time		\$3.00	\$3.00
Average Annual Occupancy	0.96	0.96	0.96
Annual Operating Budget	\$171,556	\$171,556	\$171,556
Seismic Fragility Curves			
Before Mitigation			
Slight Damage State		0.12	0.12
Moderate Damage State		0.16	0.16
Extensive Damage State		0.24	0.24
Complete Damage State		0.34	0.34
Beta		0.66	0.66
After Mitigation			
Retrofit Building Type	W2	C2	W2
Retrofit Performance Objective	LS	LS	LS
Slight Damage State		0.12	0.12
Moderate Damage State		0.16	0.16
Extensive Damage State		0.24	0.24
Complete Damage State		0.34	0.34
Beta		0.66	0.66

Data Documentation: Building Part G			
	Provide brief documentation below and/or references to other documents included with your application (with page number), but <u>ONLY for data entries in Column C</u> , which replace the default values in Column D.		
Soil Type			
Primary Structure Type			
Number of Stories			
Year Built			
Severe Vertical Irregularity			
Moderate Vertical Irregularity			
Plan Irregularity			
Pre-Code			
Post-Benchmark			
Historic Importance (if not none)			
Building Square Footage			
Building Replacement Value \$/SF			
Contents Value % of Building Value			
Displacement Costs One Time			
Displacement Costs \$/SF/month			
Fragility Curve Parameters Before Mitigation			
Fragility Curve Parameters After Mitigation			
Other Comments			



Appendix E: Schematic Seismic Retrofit Drawings

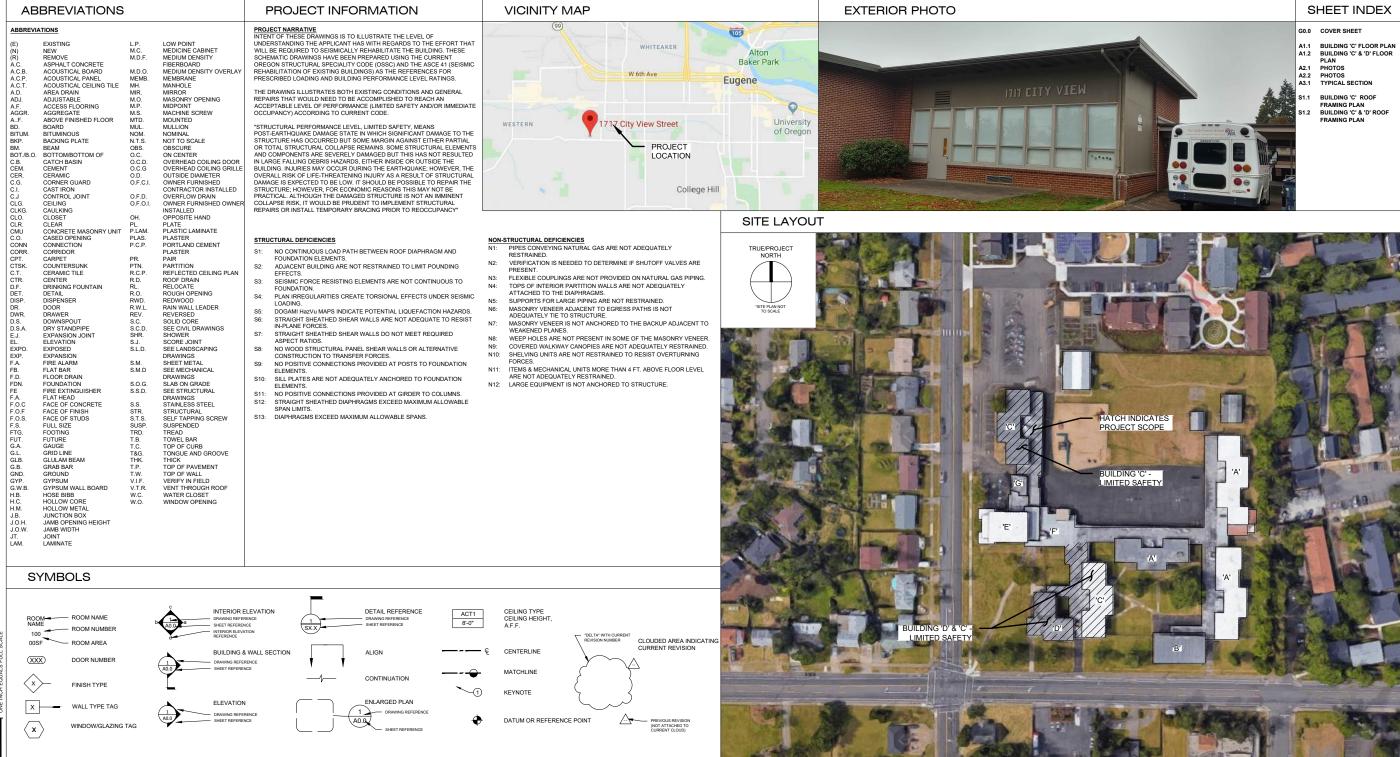
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LANE SCHOOL SEISMIC RETROFIT LANE ESD WESTMORELAND CAMPUS PHASE 1

LANE EDUCATION SERVICES DISTRICT

1717 CITY VIEW ST.

EUGENE, OREGON 97402





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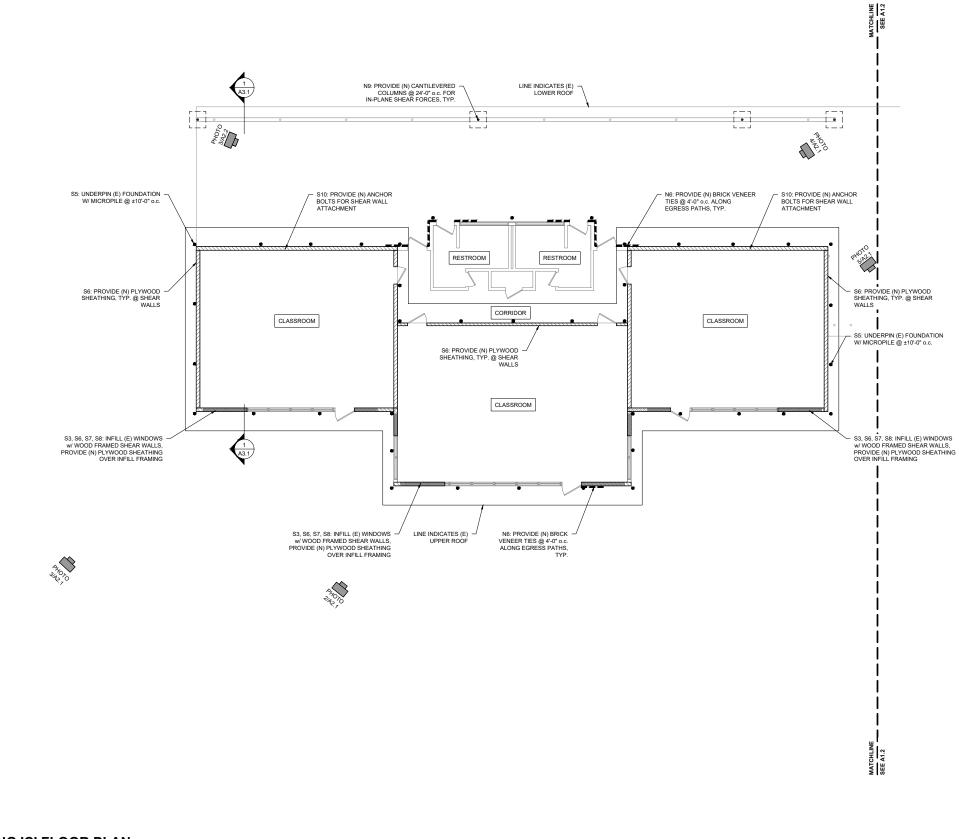
LANE ESD 1200 HIGHWAY 99 NORTH EUGENE, OREGON 97402

WESTMORELAND **CAMPUS SEISMIC** RETROFIT GRANT APPLICATION PHASE I





SR



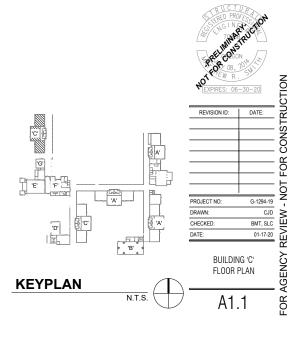
1 BUILDING 'C' FLOOR PLAN



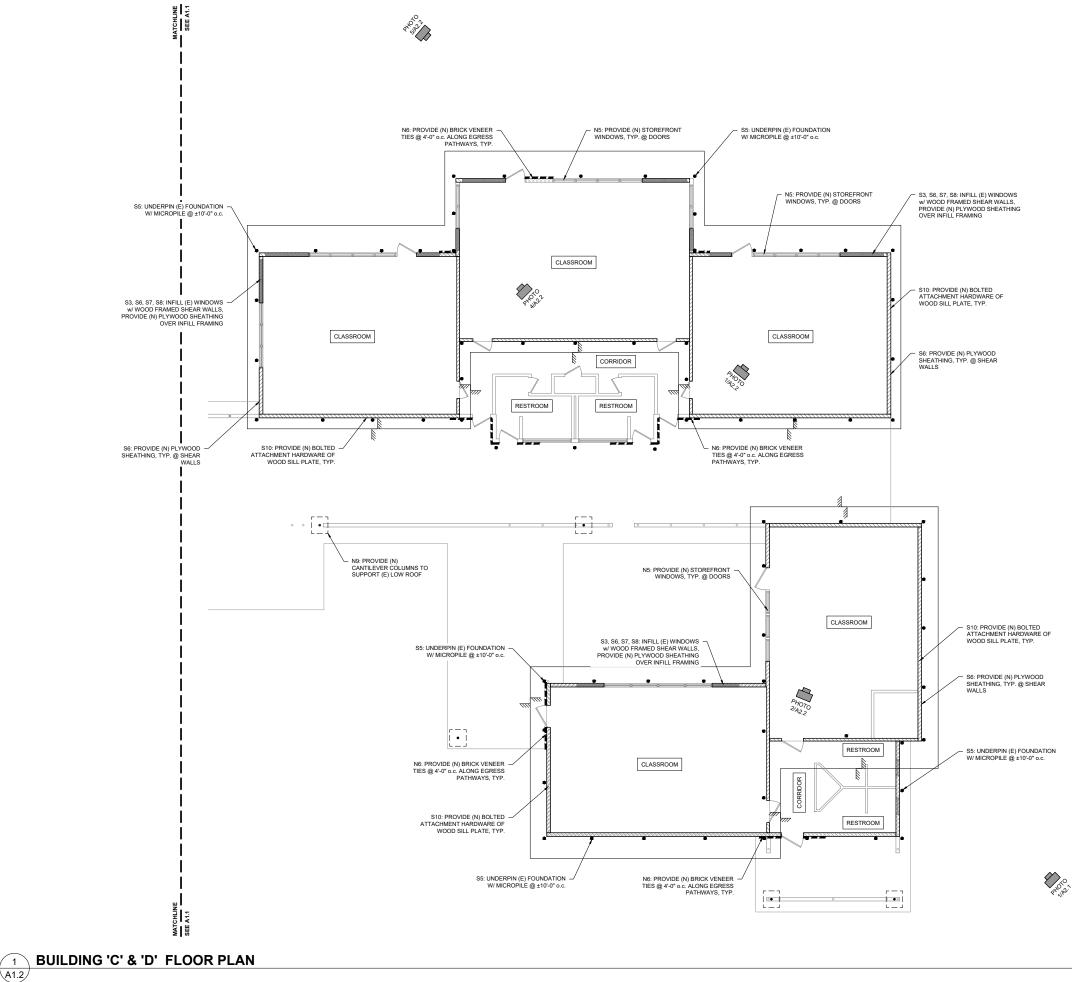
127 NW D Street, Grants Pass, Oregon 97526 | 541-479-3865

LANE ESD 1200 HIGHWAY 99 NORTH EUGENE, OREGON 97402









A1.2

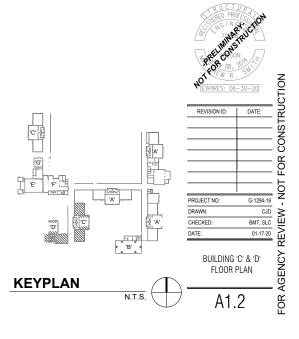
1/8" = 1'-0"



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3 PHOTO A2.1



PHOTO A2.1







N.T.S.



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3 PHOTO

N.T.S.



2 PHOTO A2.2







N.T.S.

N.T.S.

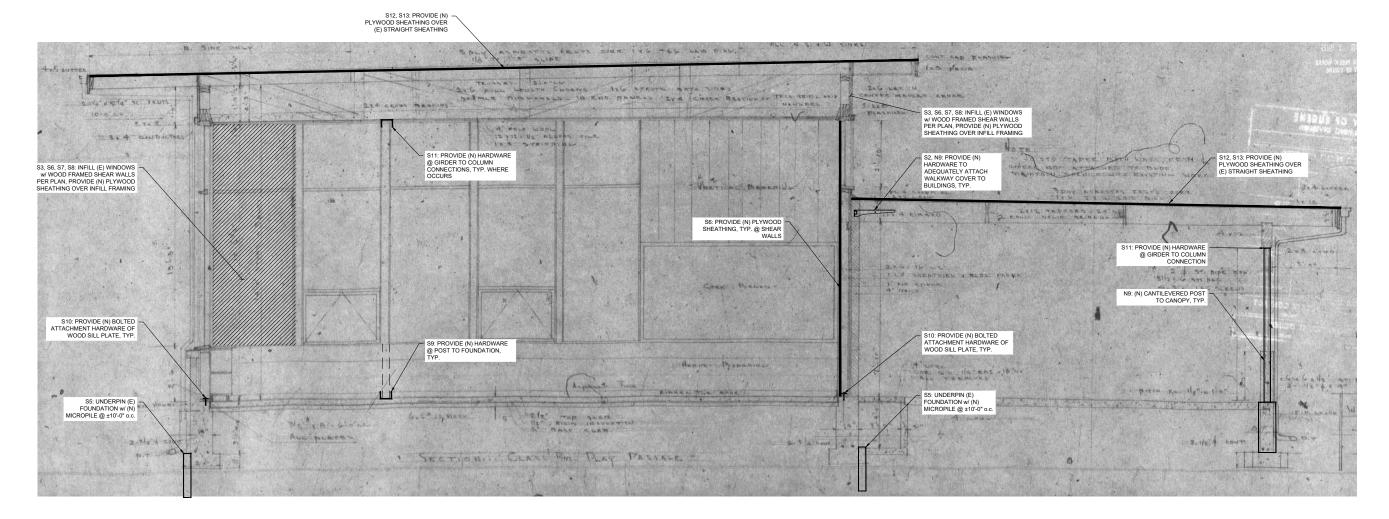


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1 TYPICAL SECTION @ CLASSROOM



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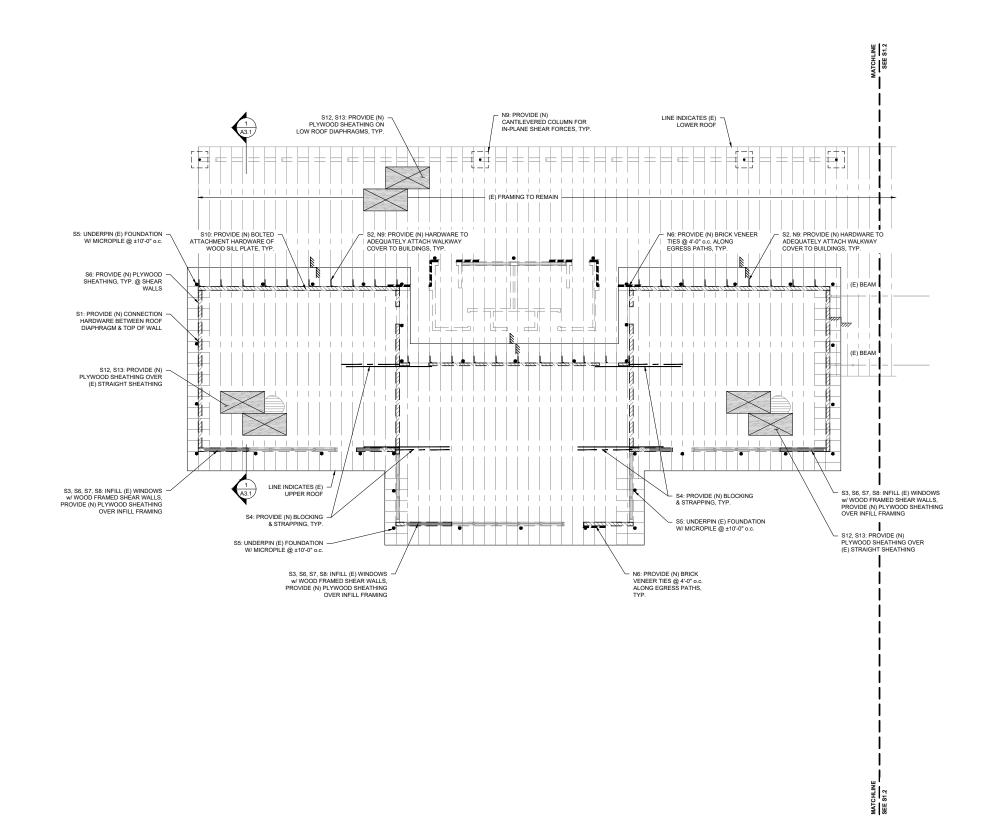
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WESTMORELAND CAMPUS SEISMIC RETROFIT GRANT APPLICATION PHASE I



1/2"= 1'-0"



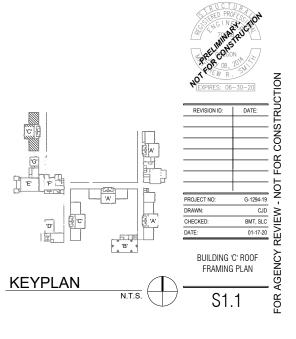




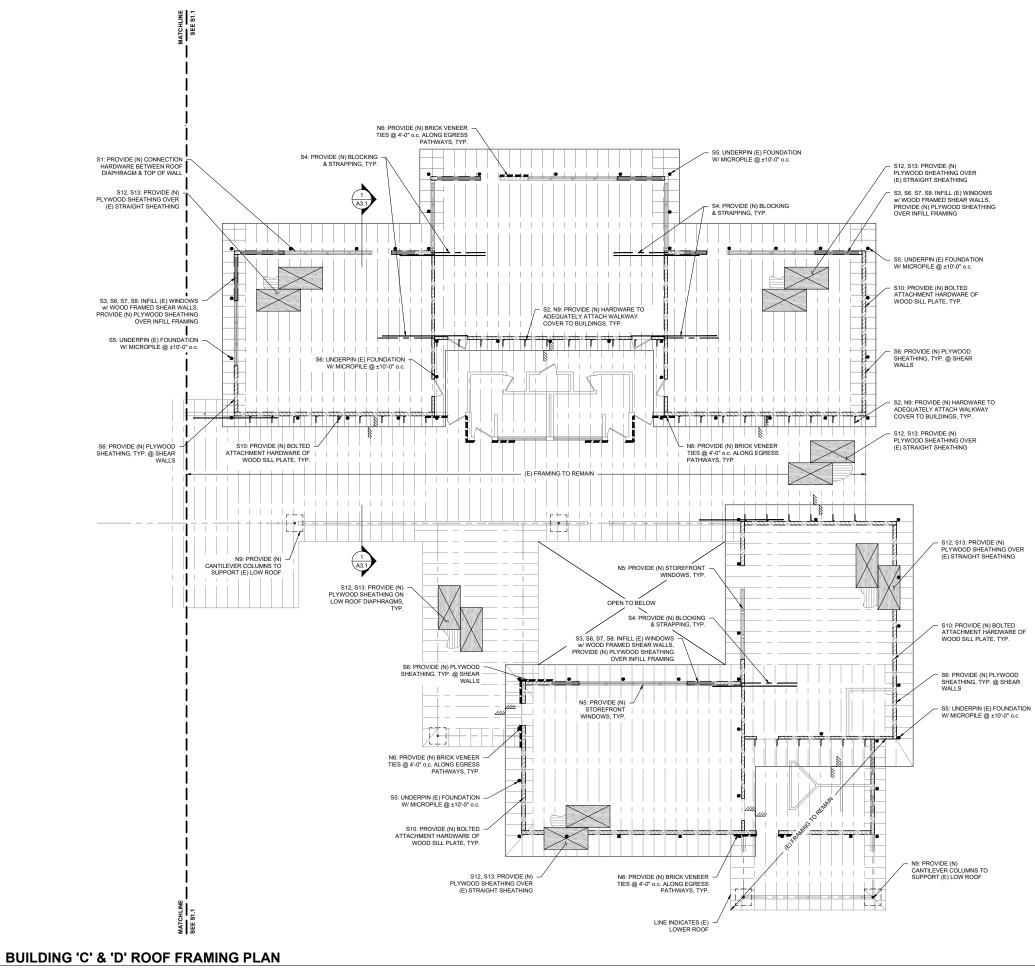
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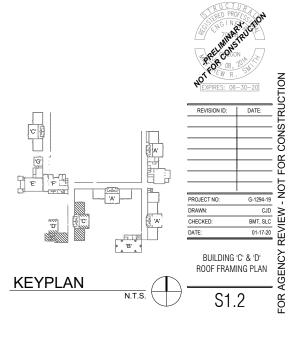




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Appendix F: RVS Score

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FEMA P-154 Data Collection Form

Westmoreland_ES A Level 1 HIGH Seismicity

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FEMA BUILDING TYPE	Do Not				(MRF)	(BR)	(LM)	(RC	(URM	(MRF)	(SW)	(URM	(TU)				URM	MH
FEMA BUILDING TYPE W2	Do Not Know							ŚW/)		(· · /	INE)			(FD)	(RD)	URM	МН
		3.6	3.2	(2.9)	2.1	2.0	2.6	SW) 2.0	INF) 1.7	1.5	2.0	INF) 1.2	1.6	1.4	(FD) 1.7		URM 1.0	MH 1.5
W2			3.2 -1.2	2.9	2.1 -1.0	2.0 -1.0	2.6 -1.1		ÌNF)	. ,		· · · ·	1.6 -1.0	1.4 -0.9	. ,	(RD)		
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1		3.6 -1.2 -0.7	-1.2 -0.7	12 07	-1.0 -0.6	-1.0 -0.6	-1.1 -0.7	2.0 -1.0 -0.6	INF) 1.7 -0.8 -0.5	1.5 -0.9 -0.5	2.0 -1.0 -0.6	1.2 -0.7 -0.4	-1.0 -0.6	-0.9 -0.5	1.7 -0.9 -0.5	(RD) 1.7 -0.9 -0.5	1.0 -0.7 -0.4	1.5 NA NA
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1}		3.6 -1.2 -0.7 -1.1	-1.2 -0.7 -1.0	12 07 10	-1.0 -0.6 -0.8	-1.0 -0.6 -0.7	-1.1 -0.7 -0.9	2.0 -1.0 -0.6 -0.7	INF) 1.7 -0.8 -0.5 -0.6	1.5 -0.9 -0.5 -0.6	2.0 -1.0 -0.6 -0.8	1.2 -0.7 -0.4 -0.5	-1.0 -0.6 -0.7	-0.9 -0.5 -0.6	1.7 -0.9 -0.5 -0.7	(RD) 1.7 -0.9 -0.5 -0.7	1.0 -0.7 -0.4 -0.4	1.5 NA NA NA
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1} Pre-Code		3.6 -1.2 -0.7 -1.1 -1.1	-1.2 -0.7 -1.0 -1.0	12 07 10 09	-1.0 -0.6 -0.8 -0.6	-1.0 -0.6 -0.7 -0.6	-1.1 -0.7 -0.9 -0.8	2.0 -1.0 -0.6 -0.7 -0.6	INF) 1.7 -0.8 -0.5 -0.6 -0.2	1.5 -0.9 -0.5 -0.6 -0.4	2.0 -1.0 -0.6 -0.8 -0.7	1.2 -0.7 -0.4 -0.5 -0.1	-1.0 -0.6 -0.7 -0.5	-0.9 -0.5 -0.6 -0.3	1.7 -0.9 -0.5 -0.7 -0.5	(RD) 1.7 -0.9 -0.5 -0.7 -0.5	1.0 -0.7 -0.4 -0.4 0.0	1.5 NA NA NA -0.1
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1} Pre-Code Post-Benchmark		3.6 -1.2 -0.7 -1.1	-1.2 -0.7 -1.0 -1.0 1.9	12 07 10 09 22	-1.0 -0.6 -0.8	-1.0 -0.6 -0.7 -0.6 1.4	-1.1 -0.7 -0.9	2.0 -1.0 -0.6 -0.7 -0.6 1.9	1.7 -0.8 -0.5 -0.6 -0.2 NA	1.5 -0.9 -0.5 -0.6 -0.4 1.9	2.0 -1.0 -0.6 -0.8 -0.7 2.1	1.2 -0.7 -0.4 -0.5 -0.1 NA	-1.0 -0.6 -0.7 -0.5 2.0	-0.9 -0.5 -0.6	1.7 -0.9 -0.5 -0.7 -0.5 2.1	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1	1.0 -0.7 -0.4 -0.4 0.0 NA	1.5 NA NA -0.1 1.2
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1} Pre-Code		3.6 -1.2 -0.7 -1.1 -1.1 1.6	-1.2 -0.7 -1.0 -1.0	12 07 10 09	-1.0 -0.6 -0.8 -0.6 1.4	-1.0 -0.6 -0.7 -0.6	-1.1 -0.7 -0.9 -0.8 1.1	2.0 -1.0 -0.6 -0.7 -0.6	INF) 1.7 -0.8 -0.5 -0.6 -0.2	1.5 -0.9 -0.5 -0.6 -0.4	2.0 -1.0 -0.6 -0.8 -0.7	1.2 -0.7 -0.4 -0.5 -0.1	-1.0 -0.6 -0.7 -0.5	-0.9 -0.5 -0.6 -0.3 2.4	1.7 -0.9 -0.5 -0.7 -0.5	(RD) 1.7 -0.9 -0.5 -0.7 -0.5	1.0 -0.7 -0.4 -0.4 0.0	1.5 NA NA NA -0.1
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1} Pre-Code Post-Benchmark Soil Type A or B		3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1	-1.2 -0.7 -1.0 -1.0 1.9 0.3	12 07 10 09 22 0.5	-1.0 -0.6 -0.8 -0.6 1.4 0.4	-1.0 -0.6 -0.7 -0.6 1.4 0.6	-1.1 -0.7 -0.9 -0.8 1.1 0.1	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6	1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5	1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3	-1.0 -0.6 -0.7 -0.5 2.0 0.6	-0.9 -0.5 -0.6 -0.3 2.4 0.4	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3	1.5 NA NA -0.1 1.2 0.3
W2 Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories)		3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2	1.2 0.7 1.0 0.9 2.2 0.5 0.1	-1.0 -0.6 -0.8 -0.6 1.4 -0.2 -0.6 0.5	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4
W2 Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories)	Know	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 <i>1.1</i>	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6	12 07 10 09 22 0.5 0.1 -0.9	-1.0 -0.6 -0.8 -0.6 1.4 -0.2 -0.6	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S _{MIN} FINAL LEVEL 1 SCORE, S _{L1}	Know	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 <i>1.1</i>	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6	12 07 10 09 22 0.5 0.1 -0.9	-1.0 -0.6 -0.8 -0.6 1.4 -0.2 -0.6 0.5 FEMA	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 15	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 AL -	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S _{MIN} FINAL LEVEL 1 SCORE, S _{L1} EXTENT OF REVIEW	Know 4 ≥ S _{MIN} :	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 <i>1.1</i> 0.7	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	-1.2 0.7 1.0 0.9 2.2 0.5 0.1 -0.9 0.7	-1.0 -0.6 -0.8 -0.6 1.4 -0.2 -0.6 0.5 FEMA OTHER	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 0.5	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT ACT	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (>	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%)	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL2 EXTENT OF REVIEW Exterior: □ Partia Interior: □ None	Know 1 ≥ S <i>MIN</i> : al ■ A	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 0.7	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	-1.0 -0.6 -0.8 -0.6 1.4 -0.2 -0.6 0.5 FEMA	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 0.5 1.5 HAZ	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That 1	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT ACT Detaile	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG RED	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (>	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 -0.3 0.3 10%)	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes	Know <i>x</i> ≥ S <i>MIN</i> : al ■ A □ \	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 0.7 All Sides /isible No	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	-1.0 -0.6 -0.8 -0.6 1.4 -0.2 -0.6 0.5 FEMA OTHER Are There Detailed St	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 A-15 Hazaro tructur	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That T al Evalu	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT ACT Detaile □ Ye	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev. own FEM	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG RED aluation	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> -	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%)	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMMN FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source:	Know <i>x</i> ≥ S <i>MIN</i> : al ■ A □ \	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 0.7 All Sides /isible No	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	-1.0 -0.6 -0.8 -0.6 1.4 -0.2 -0.6 0.5 FEMA OTHER Are There Detailed St Cut-off, Poundi	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 A-15 HAZ HAZ	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That T al Evalu ential (ur vn)	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Trigger A ation? Iless SL2	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	1.5 -0.9 -0.5 -0.4 1.9 0.4 0.0 -0.5 0.3 POT ACT Detail	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score es, score	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev. own FEM less tha	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation IA buildir n cut-off	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> -	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 -0.3 10%)	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMMN FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source:	Know 1 ≥ Smin: al ■ A □ V □ N ASS	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 0.2 -0.3 1.1 0.7	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	-1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There Detailed St Cut-off, Falling	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 HAZ HAZZ HAZZ HAZZ tructur ing pote if know	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That T al Evalu ential (ur vn)	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Trigger A ation?	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	1.5 -0.9 -0.5 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detail	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score es, other o	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev. own FEM less tha hazards	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation A buildir n cut-off present	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> ⁻	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%)	(RD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.6 0.3 	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMMN FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source:	Know 1 ≥ Smin: al ■ A □ V □ N ASS	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 0.7 All Sides /isible No	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	-1.0 -0.6 -0.8 -0.6 1.4 -0.2 -0.6 0.5 FEMA OTHER Are There Detailed St OTHER Are There Detailed St Cut-off, Falling building	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 Hazaro tructur ing pote if knov hazaro g	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS al Evalu ential (ur vn) is from ta	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Trigger A ation? allers S _{L2}	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE > cent	1.5 -0.9 -0.5 -0.4 1.9 0.4 1.9 0.4 0.0 -0.5 0.3 POT Detail	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score es, other o ed Nons	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev. own FEM less tha hazards tructura	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation A buildir n cut-off present	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> Require ng type o	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 -0.1 -0.5 -0.3 10%)	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 uilding	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMMN FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source:	Know y ≥ Smin: al A A A A A A A A A A A A A	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 0.7 All Sides Vo SUMED DOGAMI SLC	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	-1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There Detailed St OTHER Are There Detailed St Cut-off, Falling building UIDING	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 Hazaro Hazaro Hazaro g pote if knozvro g gic haze cant dal	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS al Evalu ential (ur vn) Is from ta ards or S mage/de	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Trigger A ation? Iless SL2	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE > cent F	1.5 -0.9 -0.5 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detail Yee Yee Yee Vee Detail Yee Vee Detail Yee Yee	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, unkno es, score es, other o ed Nons es, nonst	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev own FEM less tha hazards tructural I	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation A buildir n cut-off present Evalua	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> Require ng type o tion Rec	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%)	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 -0.1 -0.6 0.3 uilding ded? (ch uld be ev	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: □ Partia Interior: □ None Drawings Reviewed: □ Yes Soil Type Source: Geologic Hazards Source: Contact Person:	Know	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 0.7 All Sides Vo SUMED DOGAMI SLC	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	-1.2 0.7 1.0 0.9 2.2 0.5 0.1 -0.9 0.7 ial ered	-1.0 -0.6 -0.8 -0.6 1.4 -0.2 -0.6 0.5 FEMA OTHER Are There Detailed St OTHER Are There Detailed St Cut-off, Falling buildin Geolog	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 Hazaro Hazaro Hazaro g pote if knozvro g gic haze cant dal	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS al Evalu ential (ur vn) Is from ta ards or S mage/de	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA frigger A ation? allers S _{L2} aller adja oil Type	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE > cent F	1.5 -0.9 -0.5 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detail Yee Yee Vee Question Yee Note Vee Note No	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score es, other o ed Nons es, nonstru o, nonstru	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev. bwn FEM less tha hazards tructural h uctural h	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation A buildir n cut-off present Evalua nazards	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> Require ng type o tion Rec identified xist that	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 -0.1 -0.5 -0.3 10%)	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 -0.1 -0.6 0.3 uilding ded? (ch uld be ev	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Partia Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING Yes, Final Level 2 Score, SL2 Yes, SL2	Know	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 0.7 All Sides Vo SUMED DOGAMI SLC	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	-1.2 0.7 1.0 0.3 2.2 0.5 0.1 -0.9 0.7 ial ered	-1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There Detailed St OTHER Are There Detailed St Cut-off, Falling building UIDING	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 Hazaro Hazaro Hazaro g pote if knozvro g gic haze cant dal	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS al Evalu ential (ur vn) Is from ta ards or S mage/de	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA frigger A ation? allers S _{L2} aller adja oil Type	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE > cent F	1.5 -0.9 -0.5 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detail Yee Yee Yee Que Vee V	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, unkno es, score es, other o ed Nons es, nonst	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev. bwn FEM less tha hazards tructural h actural h uctural h	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation A buildir n cut-off present Evalua hazards azards e is not ne	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (>	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%) ad? r other but r other but	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 -0.1 -0.6 0.3 uilding ded? (ch uld be ev	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Partia Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING Yes, Final Level 2 Score, SL2 Nonstructural hazards?	Know	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 0.2 -0.3 1.1 0.7	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 Aeri Ente	-1.2 0.7 1.0 0.9 2.2 0.5 0.1 -0.9 0.7 ial erred 0 0 0	-1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There Detailed St OTHER Are There Detailed St U Cut-off, Falling building Signific the strue	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 HAZZ Hazard tructur ing pote if knov hazard g gic haza sant dai uctural	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS as That T al Evalue ential (ur vn) Is from ta ards or S mage/de system	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Trigger A ation? Iless SL2 aller adja oil Type terioratio	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE Cent F n to n	1.5 -0.9 -0.5 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detail Yee Yee Yee Que Vee No dee No	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score es, other o de Struc es, nonstru- tailed ev. o, no non	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev bwn FEM less tha hazards tructural h actural h aluation structural	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation A buildir n cut-off present Evalua nazards azards e is not ne al hazard	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (>	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%) ad? r other but sommend that sho may required	(RD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.6 0.3 	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Partia Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Yes, Final Level 2 Score, SL2 Nonstructural hazards? More information	Know	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 0.2 -0.3 1.1 0.7	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	-1.2 0.7 1.0 0.9 2.2 0.5 0.1 -0.9 0.7 ial ered 0 0 0 0 0 0 0 0 0 0 0 0 0	-1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There Detailed St OTHER Are There Detailed St U Cut-off, Falling building Signific the strue	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 Hazaro Hazaro Hazaro g gic haza scant dal uctural mote th	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS al Evalu ential (ur vn) Is from ta ards or S mage/de system e follow	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Frigger A ation? sless SL2 aller adja oil Type terioratio	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE Cent F n to n	1.5 -0.9 -0.5 -0.4 1.9 0.4 1.9 0.4 0.0 -0.5 0.3 POT Detail Petail Ye Ye Ve No Detail Ye No detail Mo mated o	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score es, other o ed Nons: es, nonstru o, nonstru tailed ev o, no non r unrelia	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev bown FEM less tha hazards tructural h actural h aluation istructura bble data	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation NA buildir n cut-off present Evalua nazards azards e is not ne al hazard	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (>	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 2.1 0.5 -0.1 0.3 10%) ad? r other but commended that sho may requ ed co Not Kr	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 uilding ded? (ch uld be ev ire mitiga DNK row	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0

FEMA P-154 Data Collection Form

Westmoreland_ES B Level 1 HIGH Seismicity

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FEMA BUILDING TYPE Do No			W2	S1	S2	S3				~~	~~						
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W2 Know Basic Score Severe Vertical Irregularity, V _{L1}	110 (0.000)	3.2 -1.2	2.9 -1.2	(MRF)			(RC	(URM			(URM		PC2 1.4 -0.9			URM 1.0 -0.7	MH 1.5 NA
W2 Know Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 VL1	3.6 -1.2 -0.7	3.2 -1.2 -0.7	2.9 -1.2 -0.7	(MRF) 2.1 -1.0 -0.6	(BR) 2.0 -1.0 -0.6	(LM) 2.6 -1.1 -0.7	(RC SW) 2.0 -1.0 -0.6	(URM INF) 1.7 -0.8 -0.5	(MRF) 1.5 -0.9 -0.5	(SW) 2.0 -1.0 -0.6	(URM INF) 1.2 -0.7 -0.4	(TU) 1.6 -1.0 -0.6	1.4 -0.9 -0.5	(FD) 1.7 -0.9 -0.5	(RD) 1.7 -0.9 -0.5	1.0 -0.7 -0.4	1.5 NA NA
W2 Know Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1	3.6 -1.2 -0.7 -1.1	3.2 -1.2 -0.7 -1.0	2.9 -1.2 -0.7 (10)	(MRF) 2.1 -1.0 -0.6 -0.8	(BR) -1.0 -0.6 -0.7	(LM) 2.6 -1.1 -0.7 -0.9	(RC SW) 2.0 -1.0 -0.6 -0.7	(URM INF) 1.7 -0.8 -0.5 -0.6	(MRF) 1.5 -0.9 -0.5 -0.6	(SW) 2.0 -1.0 -0.6 -0.8	(URM INF) 1.2 -0.7 -0.4 -0.5	(TU) 1.6 -1.0 -0.6 -0.7	1.4 -0.9 -0.5 -0.6	(FD) 1.7 -0.9 -0.5 -0.7	(RD) 1.7 -0.9 -0.5 -0.7	1.0 -0.7 -0.4 -0.4	1.5 NA NA NA
W2 Know Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 VL1	3.6 -1.2 -0.7	3.2 -1.2 -0.7	2.9 -1.2 -0.7	(MRF) 2.1 -1.0 -0.6 -0.8	(BR) 2.0 -1.0 -0.6	(LM) 2.6 -1.1 -0.7	(RC SW) 2.0 -1.0 -0.6	(URM INF) 1.7 -0.8 -0.5	(MRF) 1.5 -0.9 -0.5	(SW) 2.0 -1.0 -0.6	(URM INF) 1.2 -0.7 -0.4	(TU) 1.6 -1.0 -0.6	1.4 -0.9 -0.5	(FD) 1.7 -0.9 -0.5	(RD) 1.7 -0.9 -0.5	1.0 -0.7 -0.4	1.5 NA NA
W2 Know Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Pre-Code	3.6 -1.2 -0.7 -1.1 -1.1	3.2 -1.2 -0.7 -1.0 -1.0	2.9 -1.2 -0.7 10 -0.9	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6	(BR) -1.0 -0.6 -0.7 -0.6	(LM) 2.6 -1.1 -0.7 -0.9 -0.8	(RC SW) -1.0 -0.6 -0.7 -0.6	(URM INF) -0.8 -0.5 -0.6 -0.2	(MRF) 1.5 -0.9 -0.5 -0.6 -0.4	(SW) 2.0 -1.0 -0.6 -0.8 -0.7	(URM INF) -0.7 -0.4 -0.5 -0.1	(TU) 1.6 -1.0 -0.6 -0.7 -0.5	1.4 -0.9 -0.5 -0.6 -0.3	(FD) 1.7 -0.9 -0.5 -0.7 -0.5	(RD) 1.7 -0.9 -0.5 -0.7 -0.5	1.0 -0.7 -0.4 -0.4 0.0	1.5 NA NA NA -0.1
W2 Know Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Post-Benchmark	3.6 -1.2 -0.7 -1.1 -1.1 1.6	3.2 -1.2 -0.7 -1.0 -1.0 1.9	2.9 -1.2 -0.7 -1.0 0.9 2.2 0.5 0.1	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4	(BR) -1.0 -0.6 -0.7 -0.6 1.4	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1	(RC SW) -1.0 -0.6 -0.7 -0.6 1.9	(URM INF) -0.8 -0.5 -0.6 -0.2 NA	(MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1	(URM INF) -0.7 -0.4 -0.5 -0.1 NA	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0	1.4 -0.9 -0.5 -0.6 -0.3 2.4	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1	1.0 -0.7 -0.4 -0.4 0.0 NA	1.5 NA NA -0.1 1.2
W2 Know Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories)	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3	3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6	2.9 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6	(BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA	(RC SW) -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6	(URM INF) -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4	(MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA	1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2KnowBasic ScoreSevere Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-CodePost-BenchmarkSoil Type A or BSoil Type E (1-3 stories)Soil Type E (> 3 stories)Minimum Score, S_{MIN}	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1	3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2	2.9 -1.2 -0.7 -1.0 0.9 2.2 0.5 0.1	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5	(BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6	(RC SW) -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5	(URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	(MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2	1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4
W2 Know Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories)	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1	3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6	2.9 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 -0.2 -0.6	(BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6	(RC SW) -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5	(URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	(MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2	1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2KnowBasic ScoreSevere Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-CodePost-BenchmarkSoil Type A or BSoil Type E (1-3 stories)Soil Type E (> 3 stories)Soil Type E (> 3 stories)Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{M}$ EXTENT OF REVIEW	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 <i>I.1</i> <i>I.O</i>	3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	2.9 -1.2 -0.7 -1.0 0.9 2.2 0.5 0.1 -0.9 <i>0.7</i>	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER	(BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 -15 HAZ	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS	(RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 0.5	(URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	(MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT ACT	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED	1.4 -0.9 -0.5 -0.6 -0.3 2.4 -0.1 -0.4 -0.1 -0.4 0.2 DER	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Know Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$ EXTENT OF REVIEW Exterior: Partial	3.6 -1.2 -0.7 -1.1 -1.1 -1.1 -0.3 1.1 0.2 -0.3 1.1	3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	2.9 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There	(BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 15 HAZ	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That T	(RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 -0.1 -0.6 -0.1 -0.6 0.5 -0.1 -0.6 -0.1 -0.6 -0.1 -0.6 -0.5	(URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	(MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaild	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation	1.4 -0.9 -0.5 -0.6 -0.3 2.4 -0.1 -0.4 -0.1 -0.4 0.2 DER/	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE	(RD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10 ^c	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Know Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MI}$ EXTENT OF REVIEW Exterior: Partial Interior: None	3.6 -1.2 -0.7 -1.1 -1.1 -0.7 -1.1 -0.3 1.1 0.2 -0.3 1.1 WN: 1.0 All Sides Visible	3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	2.9 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There I Detailed St	(BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 15 HAZ	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That T al Evalue	(RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 -0.1 -0.6 0.5 CLLA	(URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	(MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile Q Yee	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, unkno	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev pwn FEM	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation IA buildin	1.4 -0.9 -0.5 -0.6 -0.3 2.4 -0.1 -0.4 -0.1 -0.4 0.2 DER/	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE	(RD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10 ^c	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Know Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MI}$ EXTENT OF REVIEW Exterior: Partial Interior: None	3.6 -1.2 -0.7 -1.1 -1.1 -1.1 -0.3 1.1 0.2 -0.3 1.1	3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	2.9 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There I Detailed St □ Poundi	(BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 -15 HAZZ Hazard ructur, ng pote	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That T al Evalue ential (un	(RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 -0.1 -0.6 0.5 CLLA	(URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	(MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile □ Yee □ Yee	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 0.3 IAL - EQUIF tural Ev pown FEM less tha	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation IA buildiin n cut-off	1.4 -0.9 -0.5 -0.6 -0.3 2.4 -0.1 -0.4 -0.4 -0.4 -0.4 -0.4 -0.4 DER/	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE	(RD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10 ^c	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W/2 Know Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MI}$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed:	3.6 -1.2 -0.7 -1.1 -1.1 -0.7 -1.1 -1.1 -0.3 1.1 0.2 -0.3 1.1 W: 1.0	3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 ▲ Aeria ■ Ente	2.9 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There I Detailed St Detailed St □ Poundi cut-off,	(BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 0.5 . -0.4 . -0.4 . -0.4 . -0.4 . -0.5 . -1.5 . -HAZZ	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That T al Evalue ential (un	(RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 -0.1 -0.6 -0.1 -0.6 0.5 DLLA	(URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 0.5 PSE	(MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaild □ Yee □ Yee □ Yee	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score es, score es, other	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 0.3 IAL - EQUIF tural Ev pown FEM less tha	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation IA buildiin n cut-off	1.4 -0.9 -0.5 -0.6 -0.3 2.4 -0.1 -0.4 -0.4 -0.4 -0.4 -0.4 -0.4 DER/	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE	(RD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10 ^c	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Know Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MI}$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source:	3.6 -1.2 -0.7 -1.1 -1.1 -1.1 -0.3 1.1 0.2 -0.3 1.1	3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 ▲ Aeria ■ Ente	2.9 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There I Detailed St Detailed St □ Poundi cut-off, □ Falling building	(BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 HAZ . HAZ . HAZ .	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.2 NA 0.6 4 CC ARDS Is That T al Evalue ential (un vn) Is from ta	(RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 0LLA irigger A ation? less SL2 ller adja	(URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 0.5 PSE > cent	(MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaild □ Yee □ Yee □ Yee □ Not	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score es, other	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev pwn FEN less tha hazards	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation IA buildin n cut-off present	1.4 -0.9 -0.5 -0.6 -0.3 2.4 -0.1 -0.4 -0.4 -0.4 -0.4 -0.4 -0.4 DER/	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE ad? r other bl	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 -0.1 -0.6 0.3 (<10^4 uilding	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 %)	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Know Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Source:	N 3.6 -1.2 -0.7 -1.1 -1.1 -0.7 -1.1 1.6 0.1 0.2 -0.3 1.1 1.6 0.1 0.2 -0.3 1.1 INN: 1.0 All Sides Visible NO ASSUMED DOGAMI SLC	3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 ▲ Aeria	2.9 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There I Detailed St □ Poundi □ Falling building □ Geolog	(BR) 2.0 -1.0 -0.6 -0.7 -0.6 -0.7 -0.6 -0.4 -0.6 0.5 HAZ HAZ HAZ 	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That T al Evalue ential (un vn) Is from ta ards or S	(RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA iss SL2 iller adja bil Type	(URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE Cent F	(MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaild □ Yee □ Yee □ No Detaild □ Yee	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ENT Con R ed Struc es, score es, other o ed Nons es, nonst	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev pwn FEN less tha hazards tructural	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation I Evaluation I Evaluation I Evaluation	1.4 -0.9 -0.5 -0.6 -0.3 2.4 -0.1 -0.4 -0.1 -0.4 0.2 DER/ ng type o	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE ad? r other bit comment that shot	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 -0.1 -0.6 0.3 (<10° uilding ded? (<i>ch</i> uild be ev	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 %)	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Know Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MI}$ Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING PER	N 3.6 -1.2 -0.7 -1.1 -1.1 -0.7 -1.1 1.6 0.1 0.2 -0.3 1.1 1.6 0.1 0.2 -0.3 1.1 INN: 1.0 All Sides Visible NO ASSUMED DOGAMI SLC	3.2 -1.2 -0.7 -1.0 1.9 0.3 0.2 -0.6 0.9 ○.2 -0.6 0.9 ■ Aeria Entee ■ Entee	2.9 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There I Detailed St □ Poundi cut-off, □ Falling building □ Geolog □ Signific	(BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.4 -0.6 0.5 HAZ2rd HAZ2rd HAZ2rd HAZ2rd is hazard ji show hazard ji show hazard ha	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That T al Evalue ential (un vn) Is from ta ards or S mage/de	(RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA is s SL2 iller adja bil Type	(URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE Cent F	(MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaild □ Yee □ Yee □ Not Detaild □ Yee □ Not	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score es, other o ed Nons es, nonstru o, nonstru	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev pwn FEM less tha hazards tructural h	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation I Evaluation I Evaluation I Evaluation I Evaluation	1.4 -0.9 -0.5 -0.6 -0.3 2.4 -0.1 -0.4 0.2 DER/ DER/ ng type o	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE ad? r other bit comment that shot	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 -0.1 -0.6 0.3 (<10° uilding ded? (<i>ch</i> uild be ev	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 %)	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Know Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MI}$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING PER Yes, Final Level 2 Score, S_{L2}	N 3.6 -1.2 -0.7 -1.1 -1.1 -0.7 -1.1 1.6 0.1 0.2 -0.3 1.1 1.6 0.1 0.2 -0.3 1.1 INN: 1.0 All Sides Visible NO ASSUMED DOGAMI SLC	3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 ○.2 -0.6 0.9 ■ Aeria Entee ■ Entee ■ Note:	2.9 -1.2 -0.7 -1.9 -0.9 0.7 0.1 -0.9 0.7 al ered	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There I Detailed St □ Poundi □ Falling building □ Geolog	(BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.4 -0.6 0.5 HAZ2rd HAZ2rd HAZ2rd HAZ2rd is hazard ji show hazard ji show hazard ha	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That T al Evalue ential (un vn) Is from ta ards or S mage/de	(RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA is s SL2 iller adja bil Type	(URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE Cent F	(MRF) 1.5 -0.9 -0.5 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile □ Yee □ Yee □ Not Detaile □ Yee □ Not 0 etaile	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ENT ENT Construction of the set	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev bown FEM less tha hazards tructural h aluation	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation I Evaluation I Evalu	1.4 -0.9 -0.5 -0.6 -0.3 2.4 -0.1 -0.4 -0.4 -0.4 -0.4 -0.2 DER/ DER/ ng type o stion Rec identified exist that ecessary	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE ad? r other bin commend that shoc may requ	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 -0.1 -0.6 0.3 (<10° uilding ded? (ch uild be ev uire mitiga	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 %)	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Know Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMNN FINAL LEVEL 1 SCORE, $S_{L1} \ge SM$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING PER Yes, Final Level 2 Score, S_{L2} Nonstructural hazards?	3.6 -1.2 -0.7 -1.1 -1.6 0.1 0.2 -0.3 1.1 w: 1.0 w: 1.0 All Sides Visible No ASSUMED DOGAMI SLC	3.2 -1.2 -0.7 -1.0 1.9 0.3 0.2 -0.6 0.9 ○.9 ○.8 ○.9 ○.9 ○.9 ○.2 -0.6 0.9 ○.9 ○.2 -0.6 ○.9 ○.2 ○.7 ○.1 ○.3 0.2 -0.6 ○.9 ○.2 ○.7 ○.1 ○.3 0.2 ·.0 ○.2 ·.0 ○.3 0.2 ·.0 ·.1 ○.2 ·.0 ·.1 ·.1 ·.1 ·.1 ·.1 ·.1 ·.1 ·.1	2.9 -1.2 -0.7 0.5 0.1 -0.9 0.7 al ered	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There I Detailed St □ Poundi cut-off, □ Falling building □ Geolog □ Signific the strue	(BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.4 -0.4 -0.4 -0.5 HAZZ , HAZZ , HAZZ , HAZZ , HAZZ , HAZZ , HAZ ,	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.2 NA 0.6 4 CC ARDS as That T al Evalu- ential (un vn) Is from ta ards or S mage/de system	(RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 -0.1 -0.6 -0.1 -0.6 0.5 LLA irigger A ation? less SL2 iller adja bil Type terioratio	(URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE > cent F n to	(MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaild □ Yee □ No de □ No de □ No	(SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT Control ed Structory ed Structor	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev pwn FEN less tha hazards tructural h aluation structurar	(TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation I Evaluation I Evalu	1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 DER/ ng type o ation Rec identified exist that accessary is identified	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE ad? r other bin comment that shoc may required	(RD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10 ^c uilding ded? (ch uild be ev uire mitiga	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 %)	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Know Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MI}$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING PER Yes, Final Level 2 Score, S_{L2}	3.6 -1.2 -0.7 -1.1 -1.6 0.1 0.2 -0.3 1.1 NN: All Sides Visible NO ASSUMED DOGAMI SLC FORME	3.2 -1.2 -0.7 -1.0 1.9 0.3 0.2 -0.6 0.9 ▲ Aeria ■ Entee D? ■ Notee verified	2.9 -1.2 -0.7 10 0.3 2.2 0.5 0.1 -0.9 0.7 0.7 al ered	(MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEMA OTHER Are There I Detailed St □ Poundi cut-off, □ Falling building □ Geolog □ Signific the strue	(BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.4 -0.4 -0.4 -0.4 -0.4 -0.5 HAZZ HAZZ HAZZ Hazard jic hazz ant data ic hazz -0.5	(LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS ARDS Is That T al Evalue ential (un vn) Is from ta ards or S mage/de system e follow	(RC SW) 2.0 -1.0 -0.7 -0.6 -0.7 -0.6 -0.1 -0.6 -0.1 -0.6 0.5 VLLAI rigger A ation? less SL2 iller adja bil Type terioratio	(URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE > cent F n to	(MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile Yee PYee No Detaile Yee No Mated o	(SW) 2.0 -1.0 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ENT ENT ENT ENT ENT ENT ENT	(URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev bown FEM less tha hazards tructural h aluation istructura ble data	(TU) 1.6 -1.0 -0.7 2.0 0.6 -0.3 NA 0.2 MO RED aluation A buildin n cut-off present I Evalua hazards azards e is not ne al hazard	1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 DER/ ng type o ation Rec identified exist that accessary is identified	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE ad? r other bindle and a short for the short f	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10° (<10° ded? (ch uilding ded? (ch uild be ev uire mitiga DNK 10%	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 %)	1.5 NA NA -0.1 1.2 0.3 -0.4 NA <i>1.0</i>

FEMA P-154 Data Collection Form

Westmoreland_ES C Level 1 HIGH Seismicity

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			and the second						SLC				D	ate/Time	e: <u>12/1</u>	7/19		
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and the second second	Contra Contra					Cathologian an	Tota	l Floor	Area (se	a. ft.):	37,320					e Year:		•
and the second second				and the				itions:		lone [<u>אין אין אין אין אין אין אין אין אין אין </u>	(ear(s) E	Built:		-		1993	
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C Sthe Little French	1		State 1	10			Adja	cency:		D Po	ounding		Falling H	azards fr	om Taller	Adjacen	t Building]
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FEMA BUILDING TYPE	Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
W2	KIIOW				(1411.17)		<u> </u>	ŚW)	ÌNF)	. ,		INF)	. ,		. ,	. ,		
Basic Score		3.6	3.2	2.9	2.1	2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, V_{L1}		-1.2	-1.2	-1.2	-1.0	-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	NA
Moderate Vertical Irregularity, V_{L1}		-0.7	-0.7 -1.0	0.7		-0.6 -0.7	-0.7 -0.9	-0.6 -0.7	-0.5 -0.6	-0.5 -0.6	-0.6 -0.8	-0.4 -0.5	-0.6 -0.7	-0.5 -0.6	-0.5 -0.7	-0.5 -0.7	-0.4 -0.4	NA
Plan Irregularity, PL1 Pre-Code		-1.1	-1.0	0.9		-0.7	-0.9	-0.7	-0.8	-0.6	-0.8	-0.5	-0.7	-0.8	-0.7	-0.7	0.4	NA -0.1
Post-Benchmark		1.6	1.9	2.2	1.4	1.4	11	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type A or B		0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories)		0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Soil Type E (> 3 stories)		-0.3	-0.6	-0.9	-0.6	-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, S _{MIN}		1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL	.1 ≥ S _{MIN} :	0.7			FEM.	A-15	4 CC)LLA	PSE	POT	ENT	IAL -	HIG	H (>'	10%)			
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		AII O' '	— • •	.							ION R			.	10			
Exterior: Parti Interior: None		All Sides √isible	Aer		Are Ther Detailed				A					Require				
Interior: None Drawings Reviewed: Yes				ereu										ng type o	r other bi	uilding		
Soil Type Source:		SUMED				ding pote ff, if knov	ential (un wn)	iess SL2	>		es, score es, other		in cut-off					
Geologic Hazards Source:		DOGAM					ds from ta	aller adja	cent				ווסטטיק					
Contact Person:		SLC			build	ing						tructura	l Evalua	tion Rec	ommen	ded? (ch	eck one)	
	DEDE						ards or S							identified				
		JRIVIE				ficant da tructural	mage/de system	ierioratic	di to					xist that				ta
Yes, Final Level 2 Score, SL					110 5	uotural	JyJICIII			de	tailed ev	aluation	is not ne	cessary		_		
	Yes										-			ls identifi				
Where info	rmation o	cannot b	e verifie	d, scre	ener shal	l note th	ne follow	ing: ES	ST = Esti	imated o	r unrelia	ble data	a <u>OR</u> I	DNK = D	o Not Kr	now		
Lessade MDE - N	Ioment-res	isting fram	ie I		inforced co	ncrete				orced maso	onry infill		= Manufa = Light me	ctured Ho			e diaphra	
	aced frame	•			near wall			"U = Tilt u									diaphragn	

FEMA P-154 Data Collection Form

Westmoreland_ES D Level 1 HIGH Seismicity

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		En				Tota	l Floor	Abov Area (so	n ff.):	• <u>1</u>	- Dei0	w Grade	•	Code	Year:		EST
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			7			Geo	logic Ha	azards:	Liquefac	tion: Yes	s/No/DN	< Lands	lide: Yes	/No/DNK	Surf. Ru	upt.: Yes/I	No/DNK
C Pithe Little French						Adja	cency:		🗌 Po	ounding		Falling H	azards fr	om Taller	Adjacent	t Building	
	(at the	-			-	Irreg	gularitie	s:		ertical (ty				(WINDOWS		ATE	
and the second s	ALL SPE	L'r m			-	_				an (type)				LOW ROOF			
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FEMA BUILDING TYPE Do Not	-	W1A	W2		S2	S3	S4	S5	C1	C2	C3	PC1	PC2	RM1	RM2	URM	МН
W2 Know				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)		(FD)	(RD)		
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-1.2 -0.7	-1.2 -0.7	-1.2 -0.7	-1.0 -0.6	-1.0 -0.6	-1.1 -0.7	-1.0 -0.6	-0.8 -0.5	-0.9 -0.5	-1.0 -0.6	-0.7 -0.4	-1.0 -0.6	-0.9 -0.5	-0.9 -0.5	-0.9 -0.5	-0.7 -0.4	NA NA
Plan Irregularity, P_{L1}	-1.1	-1.0	(1.0)	-0.8	-0.0	-0.9	-0.0	-0.5	-0.5	-0.0	-0.4	-0.7	-0.6	-0.7	-0.3	-0.4	NA
Pre-Code	-1.1	-1.0	0.9	-0.6	-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Post-Benchmark	1.6	1.9	2.2	1.4	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
			0.5	0.4	0.6	0.1						0.6	0.4			0.3	
Soil Type A or B	0.1	0.3					0.6	0.5	0.4	0.5	0.3			0.5	0.5		0.3
Soil Type A or B Soil Type E (1-3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.2 -0.3	0.2 -0.6		-0.2 -0.6	-0.4 -0.6	0.2 NA	-0.1 -0.6	-0.4 -0.4	0.0 -0.5	0.0 -0.7	-0.2 -0.3	-0.3 NA	-0.1 -0.4	-0.1 -0.5	-0.1 -0.6	-0.2 -0.2	-0.4 NA
Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S _{MIN}	0.2 -0.3 1.1	0.2	0.1 -0.9	-0.2 -0.6 0.5	-0.4 -0.6 <i>0</i> .5	0.2 NA 0.6	-0.1 -0.6 <i>0.5</i>	-0.4 -0.4 0.5	0.0 -0.5 <i>0.3</i>	0.0 -0.7 0.3	-0.2 -0.3 <i>0.3</i>	-0.3 NA 0.2	-0.1 -0.4 0.2	-0.1 -0.5 <i>0.3</i>	-0.1 -0.6 <i>0.3</i>	-0.2 -0.2 0.2	-0.4
Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$	0.2 -0.3 1.1	0.2 -0.6	0.1 -0.9	-0.2 -0.6 0.5 FEM	-0.4 -0.6 0.5 A-15 4	0.2 NA 0.6 1 CC	-0.1 -0.6 0.5	-0.4 -0.4 0.5	0.0 -0.5 0.3 POT	0.0 -0.7 0.3 ENT	-0.2 -0.3 0.3	-0.3 NA 0.2	-0.1 -0.4 0.2	-0.1 -0.5 <i>0.3</i>	-0.1 -0.6 <i>0.3</i>	-0.2 -0.2 0.2	-0.4 NA
Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S _{MIN} FINAL LEVEL 1 SCORE, S _{L1} ≥ S _{MIN} EXTENT OF REVIEW	0.2 -0.3 1.1 v: 1.0	0.2 -0.6 0.9	0.1 -0.9 <i>0</i> .7	-0.2 -0.6 0.5 FEM/	-0.4 -0.6 0.5 A-15 4	0.2 NA 0.6 4 CC	-0.1 -0.6 0.5	-0.4 -0.4 0.5 PSE	0.0 -0.5 0.3 POT	0.0 -0.7 0.3 ENT	-0.2 -0.3 0.3 IAL -	-0.3 NA 0.2 MOI	-0.1 -0.4 0.2 DER	-0.1 -0.5 0.3 ATE	-0.1 -0.6 <i>0.3</i>	-0.2 -0.2 0.2	-0.4 NA
Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S _{MIN} FINAL LEVEL 1 SCORE, S _{L1} ≥ S _{MIN} EXTENT OF REVIEW	0.2 -0.3 1.1 v: 1.0 All Sides	0.2 -0.6 0.9	0.1 -0.9 <i>0.7</i>	-0.2 -0.6 0.5 FEM	-0.4 -0.6 0.5 A-15 4 R HAZ	0.2 NA 0.6 4 CC ARDS s That T	-0.1 -0.6 0.5 DLLA	-0.4 -0.4 0.5 PSE	0.0 -0.5 0.3 POT ACT Detaile	0.0 -0.7 0.3 ENT ION R	-0.2 -0.3 0.3 IAL - EQUIF tural Ev	-0.3 NA 0.2 MOI RED aluation	-0.1 -0.4 0.2 DER	-0.1 -0.5 0.3 ATE	-0.1 -0.6 0.3 (<10°	-0.2 -0.2 0.2	-0.4 NA
Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S _{MIN} FINAL LEVEL 1 SCORE, S _{L1} ≥ S _{MIN} EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes	0.2 -0.3 1.1 v: 1.0 All Sides Visible No	0.2 -0.6 0.9	0.1 -0.9 <i>0.7</i>	-0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed	-0.4 -0.6 0.5 A-15 4 R HAZ	0.2 NA 0.6 4 CC ARDS s That T al Evalue	-0.1 -0.6 0.5 DLLA	-0.4 -0.4 0.5 PSE	0.0 -0.5 0.3 POT ACT Detaile	0.0 -0.7 0.3 ENT ION R	-0.2 -0.3 0.3 IAL - EQUIF tural Ev	-0.3 NA 0.2 MOI RED aluation	-0.1 -0.4 0.2 DER	-0.1 -0.5 0.3 ATE	-0.1 -0.6 0.3 (<10°	-0.2 -0.2 0.2	-0.4 NA
Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S _{MIN} FINAL LEVEL 1 SCORE, S _{L1} ≥ S _{MIN} EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source:	0.2 -0.3 1.1 v: 1.0 All Sides Visible No ASSUMED	0.2 -0.6 0.9	0.1 -0.9 <i>0.7</i>	-0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed 3 Detailed 3	-0.4 -0.6 0.5 A-15 4 HAZI Hazard: Structura ding pote ff, if know	0.2 NA 0.6 4 CC ARDS s That 1 s That 1 s That 1 s That 1 ntial (un n)	-0.1 -0.6 0.5 DLLA Trigger A ation?	-0.4 -0.4 0.5 PSE	0.0 -0.5 0.3 POT ACT Detaile Detaile	0.0 -0.7 0.3 ENT ION R ed Struc es, unkno es, score es, other	-0.2 -0.3 0.3 EQUIF tural Evo own FEM less tha	-0.3 NA 0.2 MOI RED aluation IA buildir n cut-off	-0.1 -0.4 0.2 DER	-0.1 -0.5 0.3 ATE	-0.1 -0.6 0.3 (<10°	-0.2 -0.2 0.2	-0.4 NA
Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S _{MIN} FINAL LEVEL 1 SCORE, S _{L1} ≥ S _{MIN} EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source:	0.2 -0.3 1.1 v: 1.0 All Sides Visible No ASSUMED DOGAMI	0.2 -0.6 0.9	0.1 -0.9 <i>0.7</i>	-0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed S Detailed S Detailed S Detailed S	-0.4 -0.6 0.5 A-15 A-15 CHAZ BHAZ BHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ C	0.2 NA 0.6 4 CC ARDS s That 1 s That 1 s That 1 s That 1 ntial (un n)	-0.1 -0.6 0.5 DLLA Trigger A ation?	-0.4 -0.4 0.5 PSE	0.0 -0.5 0.3 POT Detaile Detaile Ye Ye Ye	0.0 -0.7 0.3 ENT ION R ed Struc es, score es, other	-0.2 -0.3 0.3 IAL - EQUIF tural Evo bwn FEM less tha hazards	-0.3 NA 0.2 MOI RED aluation A buildir n cut-off present	-0.1 -0.4 0.2 DER/	-0.1 -0.5 0.3 ATE ed?	-0.1 -0.6 0.3 (<10°	-0.2 -0.2 0.2	-0.4 NA
Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL1 ≥ SMIN EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person:	0.2 -0.3 1.1 v: 1.0 All Sides Visible No Assumed Dogami SLC	0.2 -0.6 0.9	0.1 -0.9 <i>0.7</i>	-0.2 -0.6 0.5 FEM, OTHEF Are There Detailed S Detailed S Poun cut-o Fallin buildi	-0.4 -0.6 0.5 A-15 A-15 CHAZ BHAZ BHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ C	0.2 NA 0.6 4 CC ARDS s That 1 al Evalue ntial (un n) s from ta	-0.1 -0.6 0.5 DLLA Frigger A ation? less S _{L2} aller adja	-0.4 -0.4 0.5 PSE	0.0 -0.5 0.3 POT Detaile Q Yee Q Yee Q Yee D Not	0.0 -0.7 0.3 ENT ION R ed Struc es, unkno es, score es, other o ed Nons	-0.2 -0.3 0.3 IAL - EQUIF tural Ev. pwn FEM less tha hazards tructura	-0.3 NA 0.2 MOI RED aluation A buildir n cut-off present	-0.1 -0.4 0.2 DERA Require ng type o	-0.1 -0.5 0.3 ATE ed? r other bu	-0.1 -0.6 0.3 (<10°	-0.2 -0.2 0.2 %)	-0.4 NA
Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S _{MIN} FINAL LEVEL 1 SCORE, S _{L1} ≥ S _{MIN} EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING PERF	0.2 -0.3 1.1 v: 1.0 All Sides Visible No Assumed Dogami SLC	0.2 -0.6 0.9	0.1 -0.9 <i>0.7</i>	-0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed S Detailed S Poun cut-oo Fallind build Geok	-0.4 -0.6 0.5 A-15 4 HAZ A HAZ A HAZ B HAZ C C C C C C C C C C	0.2 NA 0.6 4 CC ARDS s That T al Evalue ntial (un n) s from ta rds or S nage/de	-0.1 -0.6 0.5 DLLA Trigger A ation? less S _{L2} aller adja oil Type	-0.4 -0.4 0.5 PSE	0.0 -0.5 0.3 POT Detaile Q Yee Q Yee Not Detaile Q Yee	0.0 -0.7 0.3 ENT ION R ed Struc es, unkno es, score es, other o ed Nons es, nonst	-0.2 -0.3 0.3 IAL - EQUIF tural Ev. pwn FEM less tha hazards tructural I	-0.3 NA 0.2 MOI aluation A buildir n cut-off present I Evalua nazards i	-0.1 -0.4 0.2 DER/ Require ng type o tion Rec	-0.1 -0.5 0.3 ATE ed? r other bu	-0.1 -0.6 0.3 (<10° uilding	-0.2 -0.2 0.2 %)	-0.4 NA 1.0
Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_MIN FINAL LEVEL 1 SCORE, SL1 ≥ SMIN EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING PERF Yes, Final Level 2 Score, SL2	0.2 -0.3 1.1 v: 1.0 All Sides Visible No Assumed Dogami SLC	0.2 -0.6 0.9 Aeri Ente	0.1 -0.9 0.7 al ered	-0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed S Detailed S Poun cut-oo Fallind build Geok	-0.4 -0.6 0.5 A-15 4 HAZ A HAZ B HAZ Structura ding pote ff, if know g hazards ng ogic haza	0.2 NA 0.6 4 CC ARDS s That T al Evalue ntial (un n) s from ta rds or S nage/de	-0.1 -0.6 0.5 DLLA Trigger A ation? less S _{L2} aller adja oil Type	-0.4 -0.4 0.5 PSE	0.0 -0.5 0.3 POT Detaile Petaile Yee Yee Not Detaile Vee Not Detaile	0.0 -0.7 0.3 ENT ON R ed Struc es, unkno es, score es, other ed Nons es, nonstru tailed ev	-0.2 -0.3 0.3 IAL - EQUIF tural Ev. own FEM less tha hazards tructural h actural h aluation	-0.3 NA 0.2 MOI aluation A buildir n cut-off present Evalua hazards i azards e is not ne	-0.1 -0.4 0.2 DER/ Require ng type o tion Rec identified xist that cessary	-0.1 -0.5 0.3 ATE ed? r other bu	-0.1 -0.6 0.3 (<10° uilding	-0.2 -0.2 0.2 %)	-0.4 NA 1.0
Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S _{MIN} FINAL LEVEL 1 SCORE, S _{L1} ≥ S _{MIN} EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING PERF	0.2 -0.3 1.1 v: 1.0 All Sides Visible No Assumed Dogami SLC	0.2 -0.6 0.9	0.1 -0.9 0.7 al ered	-0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed S Detailed S Poun cut-oo Fallind build Geok	-0.4 -0.6 0.5 A-15 4 HAZ A HAZ A HAZ B HAZ C C C C C C C C C C	0.2 NA 0.6 4 CC ARDS s That T al Evalue ntial (un n) s from ta rds or S nage/de	-0.1 -0.6 0.5 DLLA Trigger A ation? less S _{L2} aller adja oil Type	-0.4 -0.4 0.5 PSE	0.0 -0.5 0.3 POT Detaile Petaile Yee Yee Not Detaile Vee Not Detaile	0.0 -0.7 0.3 ENT ON R ed Struc es, unkno es, score es, other ed Nons es, nonstru tailed ev	-0.2 -0.3 0.3 IAL - EQUIF tural Ev. own FEM less tha hazards tructural h actural h aluation	-0.3 NA 0.2 MOI aluation A buildir n cut-off present Evalua hazards i azards e is not ne	-0.1 -0.4 0.2 DER/ Require ng type o tion Rec identified xist that	-0.1 -0.5 0.3 ATE ed? r other bu	-0.1 -0.6 0.3 (<10° uilding	-0.2 -0.2 0.2 %)	-0.4 NA 1.0
Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_MIN FINAL LEVEL 1 SCORE, SL1 ≥ SMIN EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING PERF Yes, Final Level 2 Score, SL2	0.2 -0.3 1.1 v: 1.0 All Sides Visible No Assumed DOGAMI SLC	0.2 -0.6 0.9 Aeri Ente	0.1 -0.9 0.7 al ered	-0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed Poun cut-o Fallin buildi Geok Signit the st	-0.4 -0.6 0.5 A-154 R HAZ/ B Hazard B Hazard ding pote ff, if know g hazard ng pogic haza iccant dan ructural s	0.2 NA 0.6 1 CC ARDS s That T al Evalue ntial (un n) s from ta rds or S nage/de system	-0.1 -0.6 0.5 DLLA	-0.4 -0.4 0.5 PSE > cent F n to	0.0 -0.5 0.3 POT Detaile 9 Ye 9 Ye 9 No Detaile 9 No 0 Detaile 9 No 0 Detaile 9 No	0.0 -0.7 0.3 ENT ON R ed Struc es, unkno es, score es, other of Nons es, nonstru tailed ev o, no non	-0.2 -0.3 0.3 IAL - EQUIF tural Ev. bwn FEM less tha hazards tructural h actural h aluation structura	-0.3 NA 0.2 MOI RED aluation A buildir n cut-off present I Evalua nazards e is not ne al hazard	-0.1 -0.4 0.2 DER/ Require ng type o tion Rec identified xist that cessary s identified	-0.1 -0.5 0.3 ATE ed? r other bu sommend that sho may requ ed	-0.1 -0.6 0.3 (<10° uilding Jed? (chu uld be ev ire mitiga	-0.2 -0.2 0.2 %)	-0.4 NA 1.0

FEMA P-154 Data Collection Form

Westmoreland_ES E Level 1 HIGH Seismicity

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FEMA BUILDING TYPE	Do Not	B W1	- Area	SCOP	S1	S2	RS, AN	ND FIN S4	S5	EVEL [/]	1 SCO C2	RE, S	<i>L1</i> PC1	PC2	RM1	RM2	URM	МН
FEMA BUILDING TYPE W2	Do Not Know		ASIC	W2			RS, AI	ND FIN	IAL LI	EVEL '	1 SCO	RE, S	L1		RM1 (FD)	RM2 (RD)	URM	МН
W2 Basic Score		W1 3.6	ASIC 3.2	W2	S1 (MRF) 2.1	S2 (BR) 2.0	RS, AN (LM) 2.6	ND FIN S4 (RC SW) 2.0	S5 (URM INF) 1.7	C1 (MRF) 1.5	1 SCO (SW) 2.0	RE, S C3 (URM INF) 1.2	L1 PC1 (TU) 1.6	PC2	(FD) 1.7	(RD) 1.7	1.0	1.5
W2 Basic Score Severe Vertical Irregularity, V _{L1}		W1 3.6 -1.2	ASIC W1A 3.2 -1.2	W2 (2.9) -1.2	S1 (MRF) 2.1 -1.0	S2 (BR) 2.0 -1.0	RS, AN S3 (LM) 2.6 -1.1	ND FIN S4 (RC SW) 2.0 -1.0	S5 (URM INF) 1.7 -0.8	C1 (MRF) 1.5 -0.9	1 SCO (SW) 2.0 -1.0	RE, S C3 (URM INF) 1.2 -0.7	L1 PC1 (TU) 1.6 -1.0	PC2 1.4 -0.9	(FD) 1.7 -0.9	(RD) 1.7 -0.9	1.0 -0.7	1.5 NA
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1}		W1 3.6	ASIC 3.2	W2 (29) 12 (07)	S1 (MRF) 2.1 -1.0 -0.6	S2 (BR) 2.0 -1.0 -0.6	RS, AN (LM) 2.6 -1.1 -0.7	ND FIN S4 (RC SW) 2.0	S5 (URM INF) 1.7 -0.8 -0.5	C1 (MRF) 1.5 -0.9 -0.5	1 SCO (SW) 2.0 -1.0 -0.6	RE, S (URM INF) 1.2 -0.7 -0.4	L1 PC1 (TU) 1.6 -1.0 -0.6	PC2 1.4 -0.9 -0.5	(FD) 1.7 -0.9 -0.5	(RD) 1.7 -0.9 -0.5	1.0	1.5
W2 Basic Score Severe Vertical Irregularity, V _{L1}		W1 3.6 -1.2 -0.7	ASIC W1A 3.2 -1.2 -0.7	W2 (29) 12 (07) 10	S1 (MRF) 2.1 -1.0	S2 (BR) 2.0 -1.0	RS, AN S3 (LM) 2.6 -1.1	ND FIN S4 (RC SW) 2.0 -1.0 -0.6	S5 (URM INF) 1.7 -0.8	C1 (MRF) 1.5 -0.9	1 SCO (SW) 2.0 -1.0	RE, S C3 (URM INF) 1.2 -0.7	L1 PC1 (TU) 1.6 -1.0	PC2 1.4 -0.9	(FD) 1.7 -0.9	(RD) 1.7 -0.9	1.0 -0.7 -0.4	1.5 NA NA
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1}		W1 3.6 -1.2 -0.7 -1.1	ASIC W1A 3.2 -1.2 -0.7 -1.0	W2 (29) 12 (07)	S1 (MRF) 2.1 -1.0 -0.6 -0.8	S2 (BR) -1.0 -0.6 -0.7	RS, AN (LM) 2.6 -1.1 -0.7 -0.9	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7	S5 (URM INF) 1.7 -0.8 -0.5 -0.6	C1 (MRF) 1.5 -0.9 -0.5 -0.6	1 SCO (SW) 2.0 -1.0 -0.6 -0.8	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7	PC2 1.4 -0.9 -0.5 -0.6	(FD) 1.7 -0.9 -0.5 -0.7	(RD) 1.7 -0.9 -0.5 -0.7	1.0 -0.7 -0.4 -0.4	1.5 NA NA NA
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1} Pre-Code		W1 3.6 -1.2 -0.7 -1.1 -1.1	ASIC W1A 3.2 -1.2 -0.7 -1.0 -1.0 -1.0	W2 -1.2 -0.7 -1.0 0.9	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6	S2 (BR) -1.0 -0.6 -0.7 -0.6	RS, AN (LM) 2.6 -1.1 -0.7 -0.9 -0.8	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6	S5 (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2	C1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4	1 SCO (SW) 2.0 -1.0 -0.6 -0.8 -0.7	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5	PC2 1.4 -0.9 -0.5 -0.6 -0.3	(FD) 1.7 -0.9 -0.5 -0.7 -0.5	(RD) 1.7 -0.9 -0.5 -0.7 -0.5	1.0 -0.7 -0.4 -0.4 0.0	1.5 NA NA NA -0.1
W2 Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories)		W1 3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2	ASIC •1.2 •0.7 •1.0 •1.0 •1.0 1.9 0.3 0.2	W2 -1.2 -0.7 -1.0 0.9 2.2 0.5 0.1	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4	RS, AN (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2	ND FIN (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1	S5 (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4	C1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0	1 SCO (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories)		W1 3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3	ASIC •1.2 •1.2 •0.7 •1.0 •1.0 1.9 0.3 0.2 •0.6	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6	S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA	S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6	S5 (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4	C1 (MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5	1 SCO (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN}	Know	W1 3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 <i>1.1</i>	ASIC •1.2 •0.7 •1.0 •1.0 •1.0 1.9 0.3 0.2	W2 -1.2 -0.7 -1.0 0.9 2.2 0.5 0.1	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5	RS, AI 33 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6	S4 (RC SW) -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6	NAL LI S5 (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	C1 (MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3	1 SCO (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3	L1 PC1 (TU) -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories)	Know	W1 3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 <i>1.1</i>	ASIC •1.2 •1.2 •0.7 •1.0 •1.0 1.9 0.3 0.2 •0.6	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEM/	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 A-154	RS, AI S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA	NAL LI S5 (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	C1 (MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT	1 SCO C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT	RE, S (UM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL -	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S _{MIN} FINAL LEVEL 1 SCORE, S _L	Know 1≥ Smin:	W1 3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 <i>1.1</i>	ASIC •1.2 •0.7 -1.0 •1.0 1.9 0.3 0.2 •0.6 0.9	W2 -1.2 -1.0 -1.0 -1.0 -1.0 -1.0 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 ∧ -154 ∧	RS, AN S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS	ND FIN S4 (RC SW) -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA	S5 (URM INF) -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	C1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT	RE, S (URM INF) -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF	L1 PC1 (TU) -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MN} FINAL LEVEL 1 SCORE, S_L EXTENT OF REVIEW Exterior: Partial Interior: None	Know 1 ≥ Smin: al al al	w1 3.6 -1.2 -0.7 -1.1 -1.1 -0.3 1.1 All Sides	ASIC •1.2 •0.7 -1.0 •1.0 1.9 0.3 0.2 •0.6 0.9	W2 -1.2 -1.0 -1.0 -1.0 -1.0 -1.0 -2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEM/ OTHER	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 A -154 CHAZA	RS, AI S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That 1	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Frigger A	S5 (URM INF) -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	C1 (MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detail	1 SCO C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 DER/	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10^4)	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL EXTENT OF REVIEW Exterior: Partia Interior: None Drawings Reviewed: Yes	I ≥ SMIN: al I Q I	w1 3.6 -1.2 -0.7 -1.1 -1.1 -0.3 1.1 All Sides /isible No	ASIC 	W2 -1.2 -1.0 -1.0 -1.0 -1.0 -1.0 -2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEM/ OTHER Are There Detailed S □	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 A-154 HAZ/ HAZ/ HAZ/ Hazard Structura ding pote	RS, AI S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.2 NA 0.6 4 CC ARDS Is That T al Evalue ential (un	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Frigger A	S5 (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 PSE	C1 (MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile □ Ye	1 SCO C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev own FEM less tha	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation IA buildin n cut-off	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 DER/ Require ng type o	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10^4)	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL EXTENT OF REVIEW Exterior: □ Partin Interior: □ None Drawings Reviewed: ■ Yes Soil Type Source:	I ≥ SMIN: al I Q I	W1 3.6 -1.2 -0.7 -1.1 -1.6 0.1 0.2 -0.3 1.1 All Sides /isible No SUMED	ASIC • 1.2 -0.7 -1.0 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 • Aeri • Enterior	W2 -1.2 -1.0 -1.0 -1.0 -1.0 -1.0 -2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEM/ OTHER Are There Detailed S	S2 (BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 A-154 Characterization Chara	RS, AI S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That 1 al Evalu ential (un //n)	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Frigger A ation?	JAL LI S5 (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 PSE	C1 (MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile □ Ye □ Ye	1 SCO C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score es, score	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev own FEM less tha	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation IA buildin n cut-off	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 DER/ Require ng type o	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10^4)	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL EXTENT OF REVIEW Exterior: □ Partii Interior: □ None Drawings Reviewed: ■ Yes Soil Type Source: Geologic Hazards Source:	1 ≥ Smin: al ■ e □	W1 3.6 -1.2 -0.7 -1.1 -1.1 -0.3 1.1 1.6 0.1 0.2 -0.3 1.1	ASIC • 1.2 -0.7 -1.0 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 • Aeri • Enterior	W2 -1.2 -1.0 -1.0 -1.0 -1.0 -1.0 -2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed S Pounc cut-of Fallin	S2 (BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 A-154 HAZA HAZA HAZA HAZA Structura ding pote f, if know g hazard	RS, AI S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS Is That 1 al Evalu ential (un //n)	ND FIN S4 (RC SW) -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Trigger A ation?	JAL LI S5 (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 PSE	C1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT ACT Detaild □ Yee □ Yee □ Yee □ Netaild	1 SCO C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score es, other	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev own FEN less tha hazards	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation IA buildin n cut-off present	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 DER/ a Require ng type o	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE r other bl	(RD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10^4 uilding	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 %)	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL EXTENT OF REVIEW Exterior: □ Partin Interior: □ None Drawings Reviewed: ■ Yes Soil Type Source:	1 ≥ Smin: al ■ e □	W1 3.6 -1.2 -0.7 -1.1 -1.6 0.1 0.2 -0.3 1.1 All Sides /isible No SUMED	ASIC • 1.2 -0.7 -1.0 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 • Aeri • Enterior	W2 -1.2 -1.0 -1.0 -1.0 -1.0 -1.0 -2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed S Pounc cut-of Fallin buildi	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 A-154 CHAZ HAZ HAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ CHAZ C	RS, AI S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS s That T al Evalu ential (un /n) s from ta	S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA rigger A ation? alless SL2	S5 (URM NF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 PSE A > cent	C1 (MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile □ Ye □ Ye □ Ye □ Ye □ Ye	1 SCO C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ENT ION R ed Struc es, score es, other o ed Nons	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev bwn FEM less tha hazards tructura	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation 1A buildin n cut-off present I Evalua	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 DER/ Require ng type o	(FD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE r other bin comment	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 -0.1 -0.6 0.3 (<10^4 uilding	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 %)	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL EXTENT OF REVIEW Exterior: □ Partii Interior: □ None Drawings Reviewed: ■ Yes Soil Type Source: Geologic Hazards Source:	Know 1 ≥ Smin: al □ e □	W1 3.6 -1.2 -0.7 -1.1 -1.6 0.1 0.2 -0.3 1.1 T.13 All Sides Visible No SSUMED DOGAMM SLC	ASIC • 1.2 -0.7 -1.0 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 • Aeri Enter	W2 -1.2 -1.0 -1.0 -1.0 -1.0 -1.0 -2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 0.4 -0.2 -0.6 0.5 FEM/ OTHER Are There Detailed S □ Pounc cut-of □ Fallin □ Geolc □ Signif	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 A-154 Hazard Structura ding pote f, if know g hazard ng gic hazar icant dar	RS, AI S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS ARDS Is That T al Evalu ential (un /n) s from ta ards or S mage/de	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Frigger A ation?	S5 (URM NF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 PSE A > cent F	C1 (MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile □ Ye □ Ye □ No Detaile	1 SCO C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, score s, score s, other o de Nons es, nonst	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev own FEM less tha hazards tructural	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation IA buildin n cut-off present I Evalua hazards	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 DER/ a Require ng type o tion Rec identified	(FD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE r other bin commender I that shot	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10^4 uilding ded? (ch uild be ev	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 %)	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL EXTENT OF REVIEW Exterior: □ Partial Interior: □ None Drawings Reviewed: □ Yes Soil Type Source: Geologic Hazards Source: Contact Person:	Know 1 ≥ Smin: al ■ / 2 □ t AS PERFC	W1 3.6 -1.2 -0.7 -1.1 -1.6 0.1 0.2 -0.3 1.1 T.13 All Sides Visible No SSUMED DOGAMM SLC	ASIC • 1.2 -0.7 -1.0 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 • Aeri Enter	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 0.4 -0.2 -0.6 0.5 FEM/ OTHER Are There Detailed S □ Pounc cut-of □ Fallin □ Geolc □ Signif	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 A-154 Hazard Structura ding pote f, if know g hazard ng	RS, AI S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS ARDS Is That T al Evalu ential (un /n) s from ta ards or S mage/de	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA rigger A ation? allers SL2 aller adja oil Type	S5 (URM NF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 PSE A > cent F	C1 (MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile □ Ye □ Ye □ Ye □ No	I SCO C2 (SW) 2.0 -1.0 -0.6 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struct es, score es, score es, nonstruct p, nonstruct	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev bown FEM less tha hazards tructural h	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation A buildin n cut-off present I Evalua hazards e	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 DER/ DER/ ng type o tion Rec identified exist that	(FD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE r other bin commender I that shot	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10^4 uilding ded? (ch uild be ev	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 %)	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL EXTENT OF REVIEW Exterior: □ Partia Interior: □ None Drawings Reviewed: □ Yes Soil Type Source: Geologic Hazards Source: Contact Person:	Know 1 ≥ Smin: al ■ / 2 □ t AS PERFC	W1 3.6 -1.2 -0.7 -1.1 -1.6 0.1 0.2 -0.3 1.1 1.6 0.1 0.2 -0.3 1.1 1.6 0.1 0.2 -0.3 1.1 T.3 All Sides Visible No SUMED DOGAMM SLC	ASIC • 1.2 -0.7 -1.0 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 • Aeri • Enter • Conternational Conternation (Conternation (Conternatio))))))	W2 -1.2 -0.7 -1.0 -2.9 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 0.4 -0.2 -0.6 0.5 FEM/ OTHER Are There Detailed S □ Pounc cut-of □ Fallin □ Geolc □ Signif	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 A-154 Hazard Structura ding pote f, if know g hazard ng gic hazar icant dar	RS, AI S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS ARDS Is That T al Evalu ential (un /n) s from ta ards or S mage/de	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA rigger A ation? allers SL2 aller adja oil Type	S5 (URM NF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 PSE A > cent F	C1 (MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile □ Ye □ Ye □ Ye □ Ye □ No Detaile	I SCO C2 (SW) 2.0 -1.0 -0.6 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Structors, unknowns, score so, other so, nonstructor, nonstructailed ev	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev bown FEM less tha hazards tructural h aluation	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation I A buildii n cut-off present I Evalua hazards azards e is not ne	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 DER/ DER/ ng type o tion Rec identified exist that	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE r other bl commend that shoc may requ	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10^4 uilding ded? (ch uild be ev	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 %)	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL EXTENT OF REVIEW Exterior: □ Partial Interior: □ None Drawings Reviewed: □ Yes Soil Type Source: Geologic Hazards Source: Contact Person:	Know	W1 3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 1.3 All Sides Visible No 	ASIC 	W2 -1.2 -0.7 -1.0 0.3 2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 0.4 -0.2 -0.6 0.5 FEM/ OTHER Are There Detailed S Pouncut-of Geold Signifi the st	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 A-154 Hazard Structura ding poted f, if know g hazard og goic haza icant dars	RS, AI S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS ARDS Is That T al Evalu ential (un vn) is from ta ards or S mage/de system	S4 (RC SW) -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Aller adja oil Type	S5 (URM) INF -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 PSE A > cent F nn to	C1 (MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile Detaile □ Ye □ Ye □ Ye □ No Detaile	1 SCO C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ENT ION R ed Structors, score es, score so, nonstructor, non non	RE, S (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev bown FEM less tha hazards tructural h aluation istructura	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation A buildin n cut-off present I Evalua hazards e is not ne al hazards	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 DER/ a Require ing type o attion Rec identified exist that ccessary ds identified	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE r other bindle commended I that show may required	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10 ^c uilding ded? (ch uild be ev uire mitiga	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 %)	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL EXTENT OF REVIEW Exterior: □ Partial Interior: □ None Drawings Reviewed: ① Yes Soil Type Source: Geologic Hazards Source: Contact Person: □ LEVEL 2 SCREENING □ Yes, Final Level 2 Score, SL Nonstructural hazards? □ Where information □	Know	W1 3.6 -1.2 -0.7 -1.1 -1.6 0.1 0.2 -0.3 1.1 1.6 0.1 0.2 -0.3 1.1 1.6 0.1 0.2 -0.3 1.1 1.3	ASIC 	W2 -1.2 -0.7 -1.0 0.3 2.2 0.5 0.1 -0.9 0.7 ial ered o lo d, scree	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 0.4 -0.2 -0.6 0.5 FEM/ OTHER Are There Detailed S Pouncut-of Geold Signifi the st	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 A-154 CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA CHAZA C	RS, AI S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS ARDS Is That T al Evalu ential (un /n) s from ta ards or S mage/de system e follow	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA ringger A ation? aller adja oil Type terioratio	S5 (URF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 PSE A S cent F on to ST = Esti	C1 (MRF) -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile Detaile □ Ye □ Ye □ Ye □ No Detaile	1 SCO C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ENT ION R ed Struc es, unknown es, score es, onnstru- tailed ev p, no non r unrelia	RE, S C3 (URF) INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL EQUIF tural Ev own FEN less tha hazards tructural h aluation ustructural ble data	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 MO RED aluation A buildin n cut-offf present I Evalua hazards e is not ne al hazards 2 <u>OR</u>	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 DER/ a Require ing type o attion Rec identified exist that ccessary ds identified	(FD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.5 0.3 ATE ad? r other bit commendation I that show may required to Not Kin	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 (<10 ^c uilding ded? (ch uild be ev uire mitiga	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 0.2 %)	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0

FEMA P-154 Data Collection Form

Westmoreland_ES F Level 1 HIGH Seismicity

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W2 Basic Score	Not W1 Know 3.6	ASIC 9	W2	S1 (MRF) 2.1	S2 (BR) 2.0	RS, AN S3 (LM) 2.6	ND FIN S4 (RC SW) 2.0	IAL LE S5 (URM INF) 1.7	C1 (MRF) 1.5	1 SCO C2 (SW) 2.0	RE, S C3 (URM INF) 1.2	L1 PC1 (TU) 1.6	PC2	(FD) 1.7	(RD) 1.7	1.0	1.5
W2 P Basic Score Severe Vertical Irregularity, V _{L1}	Not (now W1 3.6 -1.2	ASIC : W1A 3.2 -1.2	W2 (2.9) -1.2	S1 (MRF) 2.1 -1.0	S2 (BR) 2.0 -1.0	RS, AN S3 (LM) 2.6 -1.1	ND FIN (RC SW) 2.0 -1.0	S5 (URM INF) 1.7 -0.8	C1 (MRF) 1.5 -0.9	1 SCO (SW) 2.0 -1.0	RE, S, C3 (URM INF) 1.2 -0.7	L1 (TU) 1.6 -1.0	PC2 1.4 -0.9	(FD) 1.7 -0.9	(RD) 1.7 -0.9	1.0 -0.7	1.5 NA
W2 Pasic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1}	Not W1 Know 3.6	ASIC 9	W2 (29) -1.2 (07)	S1 (MRF) 2.1	S2 (BR) 2.0	RS, AN S3 (LM) 2.6	ND FIN S4 (RC SW) 2.0	IAL LE S5 (URM INF) 1.7	C1 (MRF) 1.5	1 SCO C2 (SW) 2.0	RE, S C3 (URM INF) 1.2	L1 PC1 (TU) 1.6	PC2	(FD) 1.7	(RD) 1.7	1.0	1.5
W2 P Basic Score Severe Vertical Irregularity, V _{L1}	Not (now W1 3.6 -1.2 -0.7 -0.7	ASIC 3 W1A 3.2 -1.2 -0.7	W2 (2.9) -1.2	S1 (MRF) 2.1 -1.0 -0.6	S2 (BR) 2.0 -1.0 -0.6	RS, AN (LM) 2.6 -1.1 -0.7	ND FIN S4 (RC SW) 2.0 -1.0 -0.6	S5 (URM INF) 1.7 -0.8 -0.5	C1 (MRF) 1.5 -0.9 -0.5	1 SCO (SW) 2.0 -1.0 -0.6	RE, S, (URM INF) 1.2 -0.7 -0.4	L1 PC1 (TU) 1.6 -1.0 -0.6	PC2 1.4 -0.9 -0.5	(FD) 1.7 -0.9 -0.5	(RD) 1.7 -0.9 -0.5	1.0 -0.7 -0.4	1.5 NA NA
W2 Pasic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1}	Not (now W1 3.6 -1.2 -0.7 -1.1	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9	W2 2.9 1.2 0.7 1.0	S1 (MRF) 2.1 -1.0 -0.6 -0.8	S2 (BR) -1.0 -0.6 -0.7	S3 (LM) 2.6 -1.1 -0.7 -0.9	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7	IAL LE (URM INF) 1.7 -0.8 -0.5 -0.6	C1 (MRF) 1.5 -0.9 -0.5 -0.6	C2 (SW) 2.0 -1.0 -0.6 -0.8	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA	PC1 (TU) 1.6 -1.0 -0.6 -0.7	PC2 1.4 -0.9 -0.5 -0.6	(FD) 1.7 -0.9 -0.5 -0.7	(RD) 1.7 -0.9 -0.5 -0.7	1.0 -0.7 -0.4 -0.4	1.5 NA NA -0.1 1.2
W2 Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1} Pre-Code Post-Benchmark Soil Type A or B	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -1.1 0.1 0.1	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6	S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1	ND FIN (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6	JAL LE S5 (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5	C1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4	C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3	1.5 NA NA -0.1 1.2 0.3
W2PBasic ScoreSevere Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-CodePost-BenchmarkSoil Type A or BSoil Type E (1-3 stories)	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -0.1 0.1 0.2	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4	S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2	ND FIN (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1	JAL LE S5 (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4	C1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0	1 SCO (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4
W2PBasic ScoreSevere Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-CodePost-BenchmarkSoil Type A or BSoil Type E (1-3 stories)Soil Type E (> 3 stories)	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -0.1 0.1 0.2 -0.3 -0.3	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6	S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA	ND FIN S4 (RC SW) -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6	S5 (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4	C1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5	C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA	PC2 1.4 -0.9 -0.5 -0.6 0.3 2.4 0.4 -0.1 -0.4	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2PBasic ScoreSevere Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-CodePost-BenchmarkSoil Type A or BSoil Type E (1-3 stories)Soil Type E (> 3 stories)Minimum Score, S_{MIN}	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -0.1 0.1 0.2 -0.3 1.1	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5	RS, AN 33 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 1.9 0.6 -0.1 -0.6 0.5	S5 (URM INF) -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 0.5	C1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3	C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3	RE, S, (URM INF) -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4
W2PBasic ScoreSevere Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-CodePost-BenchmarkSoil Type A or BSoil Type E (1-3 stories)Soil Type E (> 3 stories)Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge$	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -0.1 0.1 0.2 -0.3 1.1	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEM/	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 A-154	S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA	S5 (URM INF) -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 0.5	VEL 1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT	C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL -	PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2PBasic ScoreSevere Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-CodePost-BenchmarkSoil Type A or BSoil Type E (1-3 stories)Soil Type E (> 3 stories)Soil Type E (> 3 stories)Minimum Score, S_{MN} FINAL LEVEL 1 SCORE, $S_{L1} \ge$ EXTENT OF REVIEW	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -0.3 1.1 0.2 -0.3 1.1 Smin: 0.7	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	W2 -1.2 -1.9 -1.2 -1.9 2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 -0.2 -0.6 0.5 FEM/ OTHEF	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 A -154 A -154 A + 154	S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA	Image: Non-State Non-State 1000000000000000000000000000000000000	C1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT ACT	C2 (SW) 2.0 -1.0 -0.6 -0.7 2.1 0.5 0.0 -0.7 2.1 0.5 0.0 -0.7 0.0	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF	PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG RED	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (>	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%)	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2PBasic ScoreSevere Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-CodePost-BenchmarkSoil Type A or BSoil Type E (1-3 stories)Soil Type E (> 3 stories)Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge$	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -1.6 0.1 0.2 -0.3 1.1 Smix: 0.7	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEM/	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 A-154 C HAZ/A HAZ/A	RS, AN S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.2 NA 0.6 4 CCC ARDS s That 1	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Frigger A	Image: Non-State Non-State 1000000000000000000000000000000000000	VEL 1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile	C2 (SW) -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ON R ed Struc	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev.	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (>	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%)	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 P Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -0.1 0.2 -0.3 1.1 5 WN: 0.7	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 Aeri	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEM/ OTHEF Are Ther Detailed	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 A-154 C HAZ/A HAZ/A	RS, AN S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS s That T al Evalu	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Trigger A ation?	IAL LE S5 (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	VEL 1 C1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT ACTI Detaile □ Yee	C2 (SW) -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ON R ed Struc	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Evo wm FEM	PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG RED aluation IA buildin	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> Require ng type o	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%)	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 P Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL1 ≥ EXTENT OF REVIEW Exterior: □ Partial Interior: □ None Drawings Reviewed: ▼ Yes Soil Type Source: □	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -1.6 0.1 0.2 -0.3 1.1 Smix: 0.7	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 Aeri Ente	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed □ Poun cut-oi	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 A -154 A -15	RS, AN S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.2 NA 0.6 4 CC ARDS s That 1 al Evalu ential (un (n)	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Frigger A ation?	Interpretation Interpretation 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	VEL 1 C1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile □ Yee □ Yee □ Yee □ Yee	C2 (SW) 2.0 -1.0 -0.6 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT Ion R ed Struct es, score s, score s, other	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Evo wm FEM less tha	PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG RED aluation IA buildin n cut-off	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> - Require ng type o	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%)	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 P Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MN} FINAL LEVEL 1 SCORE, $S_{L1} \ge$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source:	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -1.6 0.1 0.2 -0.3 1.1 Smin: 0.7	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 Aeri Ente	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed □	S2 (BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 A-154 CHAZ/A	RS, AN S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.2 NA 0.6 4 CC ARDS s That 1 al Evalu ential (un (n)	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA Frigger A ation?	Interpretation Interpretation 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 PSE	VEL 1 C1 (MRF) 1.5 -0.9 -0.5 -0.4 1.9 0.4 0.0 -0.5 0.3 POT ACTI Detaile □ Yee □ Yee □ No	C2 (SW) 2.0 -1.0 -0.6 -0.7 2.1 0.5 0.0 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struct es, score es, other	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Evo wwn FEM less tha hazards	PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation IA buildin n cut-off present	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> - Require ng type o	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 -0.1 -0.5 0.3 10%) d? r other bu	(RD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.6 0.3 uilding	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 P Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL1 ≥ EXTENT OF REVIEW Exterior: □ Partial Interior: □ None Drawings Reviewed: ▼ Yes Soil Type Source: □	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -1.6 0.1 0.2 -0.3 1.1 Smix: 0.7	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 Aeri Ente	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed □ Poun cut-o' □ Fallin buildi	S2 (BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 A-154 CHAZ/A BHA BHAZ/A BHA BHA BHA BHA BHA BHA BHA BHA BHA BH	RS, AN S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS s That T al Evalu ential (un rn) s from ta	S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.5 DLLA Trigger A ation? allers SL2	Intervention Intervention 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 0.5 -0.4 -0.5 -0.4 0.5 -0.4 0.5 -0.4 0.5 -0.4 0.5 -0.4 0.5 -0.5 PSE -0.4	VEL 1 C1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaild □ Ye □ Ye □ No Detaild	C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ENT ION R ed Structors, score states, score states, other -states, other	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev. own FEM less tha hazards tructura	L1 PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation IA buildir n cut-off present I Evalua	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> - Require ng type o	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%) d? r other but commend	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 uilding	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
W2 P Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MN} FINAL LEVEL 1 SCORE, $S_{L1} \ge$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source:	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -1.6 0.1 0.2 -0.3 1.1 Smix: 0.7 ■ All Sides No	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 Aerit	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 FEM/ OTHEF Are Therr Detailed □ Poun cut-ol □ Fallin buildi □ Geold	S2 (BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 A-154 CHAZ/A	RS, AN S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS s That T al Evalu whitial (um rn) s from ta rds or S	S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.5 DLLA rigger A ation? allers SL2 aller adja oil Type	Image: Non-State State State (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 -0.4 -0.5 PSE Cent F	VEL 1 C1 (MRF) 1.5 -0.9 -0.5 -0.4 1.9 0.4 0.0 -0.5 0.3 POT ACTI Detaile □ Yee □ No Detaile □ Yee □ No Detaile □ Yee	C2 (SW) 2.0 -1.0 -0.6 -0.7 2.1 0.5 0.0 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struct es, score es, other o constant ed Nons es, nonstant	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Evo pown FEM less tha hazards tructural	PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation IA building n cut-off present I Evaluation	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> Require ng type o tion Rec identified	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%) d? r other but commend that sho	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 -0.1 -0.6 0.3 uilding ded? (chu uld be ev	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 H Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Contact Person:	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -1.6 0.1 0.2 -0.3 1.1 Smix: 0.7 ■ All Sides No	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 Aerit	W2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 0.4 -0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed □	S2 (BR) 2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 A-154 A-154 CHAZ/A BHAZ	RS, AN S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS s That T al Evalu whitial (un rn) s from ta rds or S mage/de	S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.5 DLLA rigger A ation? allers SL2 aller adja oil Type	Image: Non-State State State (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 -0.4 -0.5 PSE Cent F	VEL 1 C1 (MRF) 1.5 -0.9 -0.5 -0.4 1.9 0.4 0.0 -0.5 0.3 POT ACTI Detaile □ Yee □ Not Detaile □ Yee □ Not	C2 (SW) 2.0 -1.0 -0.6 -0.7 2.1 0.5 0.0 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struct es, score es, other o ed Nons: es, nonstru o, nonstru	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Evo pown FEM less tha hazards tructural h	PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation IA building n cut-off present I Evaluation hazards azards	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> Require ng type o tion Rec identified exist that i	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%) d? r other but commend that sho	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 -0.1 -0.6 0.3 uilding ded? (chu uld be ev	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 P Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MN} FINAL LEVEL 1 SCORE, $S_{L1} \ge$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING PE	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -1.6 0.1 0.2 -0.3 1.1 SMIN: 0.7	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 Aeri Ente	w2 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 0.4 -0.2 -0.6 0.5 FEM/ OTHEF Are There Detailed □	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 A-15 4 Hazard Structura ding pote f, if know g hazard ng gic haza icant dan	RS, AN S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS s That T al Evalu whitial (un rn) s from ta rds or S mage/de	S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.5 DLLA rigger A ation? allers SL2 aller adja oil Type	Image: Non-State State State (URM INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 -0.4 -0.5 PSE Cent F	VEL 1 C1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaild □ Yee □ Noc Detaild □ Yee □ Noc Detaild □ Yee □ Noc □ Yee □ Noc □ Yee	C2 (SW) 2.0 -1.0 -0.6 -0.7 2.1 0.5 0.0 -0.7 8, score ed Struct es, unknow es, score es, other o o, score es, nonstructailed ev	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Ev. wm FEM less tha hazards tructural h aluation	PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation IA building n cut-off present I Evaluation hazards azards eis	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> C Require ng type o tion Rec identified exist that is cessary	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%) d? r other but commended that shoo may requ	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 -0.1 -0.6 0.3 uilding ded? (chu uld be ev	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 P Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pian Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Contact Person: LEVEL 2 SCREENING PE Yes, Final Level 2 Score, S_{L2} Nonstructural hazards? Yes	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -1.1 0.7 -1.1 -1.1 -0.3 1.1 0.2 -0.3 1.1 SMIN: 0.7	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 Aeri Ente	w2 -1.2 -0.7 -1.0 0.9 2.2 0.5 0.1 -0.9 0.7	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.5 FEM/ OTHEF Are There Detailed □ Poun cut-oi □ Fallin buildi Geold Signit the st	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 A -154 A -155 A	RS, AN S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CCC ARDS s That T al Evalue ential (un rn) s from ta rds or S mage/de system	S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 0.6 0.7 -0.6 1.9 0.6 0.1 -0.6 0.5 DLLA Aation? aller adja oil Type terioratio	INF 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 PSE Cent F n to	VEL 1 C1 (MRF) 1.5 -0.9 -0.5 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile □ Yee □ Not Detaile □ Yee □ Not □ Not	C2 (SW) 2.0 -1.0 -0.6 -0.7 2.1 0.5 0.0 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struct es, score es, score es, nonstruct p, nonstruct p, nonstruct p, no non	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Evo wm FEM less tha hazards tructural hazards tructural hazards	PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation Abuilding n cut-off present HEvaluation hazards azards exards exards is not neal	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> Require ng type o tion Rec identified exist that be cessary Is identified	(FD) 1.7 -0.9 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%) d? r other but that sho may requ ed	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 -0.1 -0.6 0.3 uilding ded? (chu uid be ev ire mitiga	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0
W2 H Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, $S_{L1} \ge$ EXTENT OF REVIEW Exterior: Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person:	Not (now W1 3.6 -1.2 -0.7 -1.1 -1.1 -1.1 0.7 -1.1 -1.1 -0.3 1.1 0.2 -0.3 1.1 SMIN: 0.7	ASIC 3 W1A 3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 0.9 Aeri Ente	w2 -1.2 -0.7 -1.9 0.9 2.2 0.5 0.1 -0.9 0.7 0.7 0.7 d, scre	S1 (MRF) 2.1 -1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.5 FEM/ OTHEF Are There Detailed □ Poun cut-oi □ Fallin buildi Geold Signit the st	S2 (BR) -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 A -154 C A -154 C A -154 C C C C C C C C C C	RS, AN S3 (LM) 2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 4 CC ARDS s That T al Evalu ential (un (n) s from ta s from ta system e follow	ND FIN S4 (RC SW) 2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 1.9 0.6 -0.1 -0.6 0.5 DLLA frigger A ation? aller adja oil Type terioratio	INF 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.5 PSE Cent F n to	VEL 1 (MRF) 1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 POT Detaile Yee Q Yee No Detaile Yee No detaile Yee No detaile Mo mated o	I SCO C2 (SW) 2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 2.1 0.5 0.0 -0.7 0.3 ENT ION R ed Struc es, other o ed Nons' es, nonstructailed evo, nonstructailed evo, no non r unrelia	RE, S, (URM INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 IAL - EQUIF tural Evo wm FEM less tha hazards tructural h aluation istructura ble data	PC1 (TU) 1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 HIG aluation IA buildir n cut-off present I Evalua hazards e is not ne al hazards OR	PC2 1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 H (> Require ng type o tion Rec identified exist that be cessary Is identified	(FD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 10%) d? r other but that sho may requ ed [o Not Kr	(RD) 1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 uilding ded? (ch. uld be ev ire mitiga DNK	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2 0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA 1.0

FEMA P-154 Data Collection Form

Westmoreland_ES G Level 1 HIGH Seismicity

						Add	ress: _	717 CITY VIE	W STREET								
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															Built:	r	EST
	Nest Contra	01020				Tota	al Floor	Area (so	t. ft.):	• <u>1</u>	_ Delo	w Glaue	e:		Year:	1950 L	
		17		St.			itions:] Yes, Y		uilt:					
	i .	and the second				Occ	upancy	Ass	embly	Comme	rcial	Emer. S	Services	🗆 Hi	storic	Shelt	ter
		and and	and the second			-			strial	Office		School			overnmer	nt	
							-	Utili	·	Wareho			ntial, #Ur				
						Soll	Туре:	□A Hard	□B Avg	Den:			_		NK DNK, ass	ume Type	D.
	C. Start	The second	SHE I					Rock	Rock	Soi				Soil			
			1			Geo	logic Ha	azards:	Liquefac	tion: Yes	s/No/DN	< Lands	lide: Yes	/No/DNK	Surf. Ru	upt.: Yes/I	No/DNK
C Stitle Little French			10			Adja	acency:		🔳 Po	ounding		Falling H	lazards fr	om Taller	Adjacen	t Building	
		1 - 1				Irreg	gularitie	s:		ertical (ty an (type)	•	ity)	LOW ROOF				
1 mg 2	The second		-	A		Exte	erior Fal	ling	U	nbraced	Chimney	/S	🗌 Hea	avy Clado	ling or H	eavy Ven	neer
C.C.	,dq ⁴					Haz	ards:			arapets ther:			🗌 Арр	pendages	i		
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		D			1		Addition	al sketch	es or con	nments c	on separa	ate page					
	В	ASIC	SCO	RE, MO	DIFIE	RS, Al	ND FIN	IAL LE	EVEL	1 SCO	RE, S	L1					
FEMA BUILDING TYPE Do Not URM Know		W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	(1.0)	1.5
Severe Vertical Irregularity, V _{L1}	-1.2	-1.2	-1.2	-1.0	-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	NA
Moderate Vertical Irregularity, <i>V</i> _{L1} Plan Irregularity, <i>P</i> _{L1}	-0.7 -1.1	-0.7 -1.0	-0.7 -1.0	-0.6 -0.8	-0.6 -0.7	-0.7 -0.9	-0.6 -0.7	-0.5 -0.6	-0.5 -0.6	-0.6 -0.8	-0.4 -0.5	-0.6 -0.7	-0.5 -0.6	-0.5 -0.7	-0.5 -0.7	0.4	NA NA
Pre-Code	-1.1	-1.0	-0.9	-0.6	-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Post-Benchmark	1.6	1.9	2.2	1.4	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type A or B Soil Type E (1-3 stories)	0.1 0.2	0.3 0.2	0.5 0.1	0.4 -0.2	0.6 -0.4	0.1 0.2	0.6	0.5 -0.4	0.4 0.0	0.5 0.0	0.3 -0.2	0.6 -0.3	0.4 -0.1	0.5 -0.1	0.5 -0.1	0.3 -0.2	0.3 -0.4
Soil Type E (> 3 stories)	-0.3	-0.6	-0.9	-0.2	-0.4	NA	-0.6	-0.4	-0.5	-0.7	-0.2	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, S _{MIN}	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$: 0.6			FEMA	۱ -15	4 CC	DLLA	PSE	POT	ENT	IAL -	HIG	H (>	10%)			
EXTENT OF REVIEW				OTHER	HAZ	ARDS			ACT	ION R	EQUIF	RED					
	All Sides Visible	Aeri		Are There Detailed S				\					Require				
	No		ereu							es, unkno es, score				r other bi	uilding		
	ASSUMED				ing pot , if knov	ential (ur wn)	1185 OL2	-		es, score es, other							
Geologic Hazards Source:	DOGAM			🗌 Falling	hazaro	ds from ta	aller adja	cent	No.								
Contact Person:	SLC			buildir Geolo		ards or S	oil Type	F	Detaile	ed Nons	tructura	l Evalua	tion Rec	commend	ded? (ch	eck one)	
LEVEL 2 SCREENING PERF	ORME	D?	Ţ	Signif	cant da	mage/de	terioratic	n to						I that sho			
Yes, Final Level 2 Score, SL2		N N	0			system				o, nonstru tailed ev				may requ	ure mitiga	ation, but	a
Nonstructural hazards?		N	0										ls identifi	ed [] DNK		
Where information	cannot b	e verifie	d, scre	ener shall	note th	ne follow	ing: ES	GT = Esti	mated o	r unrelia	ble data	<u> 0R</u>	DNK = D	o Not Kr	iow		